# RECLANATION Managing Water in the West

Altus Reservoir 2007 Sedimentation Survey





U.S. Department of the Interior Bureau of Reclamation Technical Service Center Denver, Colorado

# Altus Reservoir 2007 Sedimentation Survey

prepared by

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Reclamation surveyed Altus Reservoir in November 2006, June 2007, and February 2008 to develop updated reservoir topography and compute the present storage-elevation relationship (area-capacity tables). The underwater survey conducted between water surface elevations 1,559.2 and 1,559.5 (feet), used sonic depth recording equipment interfaced with a real-time kinematic (RTK) global positioning system (GPS) that provided continuous sounding positions throughout the underwater portion of the reservoir covered by the survey vessel. The above-water topography was obtained by digitizing reservoir contour lines from the U.S. Geological Survey quadrangle (USGS quad) maps of the reservoir area and adjusting them with the limited RTK GPS land survey points collected in November 2006 and February 2008. The RTK GPS and USGS quad contour data were also used to develop contours where boat access was not possible due to thick vegetation and shallow water conditions. This study assumed no change since the 1967 survey at elevation 1,565.0 and above. The surface areas and resulting capacity data from elevation 1,565.0 to 1,565.0 were computed by linear interpolation. Accurate mapping of the upper reservoir contours would require aerial data collection when the vegetation foliage was minimal and during low reservoir conditions.					
As of June 2007, at elevation 1,559.0, the surface area was 6,273 acres with a total capacity of 128,919 acre-feet. Since the December 1940 dam closure, about 27,749 acre-feet of change has occurred (417 acre-feet per year average) below elevation 1,559.0 due to sediment deposition, resulting in a 17.7 percent loss in reservoir volume.					
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# Altus Reservoir 2007 Sedimentation Survey

## Introduction

Altus Dam and Reservoir are principal features of the W.C. Austin (formerly Altus) Project in Greer and Kiowa Counties located in southwestern Oklahoma (Figure 1). The project is operated and maintained to provide water storage for irrigation and flood control on the North Fork of the Red River. The project also provides fish and wildlife conservation benefits, municipal water, and recreation facilities. The reservoir, located about 18 miles north of Altus, is formed by a dam across the North Fork of the Red River and earthen dikes at five low points along the reservoir rim. The dam, reservoir, and irrigation distribution system are operated by the Lugert-Altus Irrigation District.

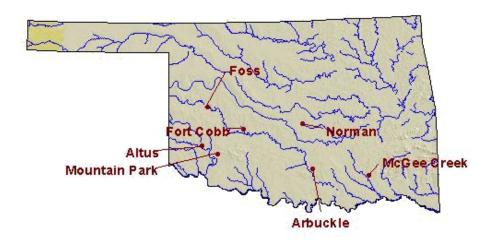


Figure 1 - Reclamation Reservoirs Located in Oklahoma.

East Dike is 10,240 feet long and 27 feet high, Lugert Dike 4,210 feet long and 47 feet high, South Dike 330 feet long and 35 feet high, and North Dike 935 feet long and 27 feet high with all crests at elevation 1,571.0 feet. The Auxiliary or

Elevations in feet. All elevations based on the original project datum established by Reclamation that is near the National Geodetic Vertical Datum of 1929 (NGVD29) and around 0.5 feet lower than the North American Vertical Datum of 1988 (NAVD88). Top of parapet wall, elevation 1,566.67.

Santa Fe Railroad Dike is 5,000 feet long and 25 feet high with crest elevation 1,569.0.

Altus Dam is a partially curved concrete gravity structure with granite masonry except on the downstream face of the overflow section (Figure 2). The dam's dimensions are:

Hydraulic height 62.3 feet Structural height 110 feet Crest length 1,112 feet Crest elevation 1,564.0 feet

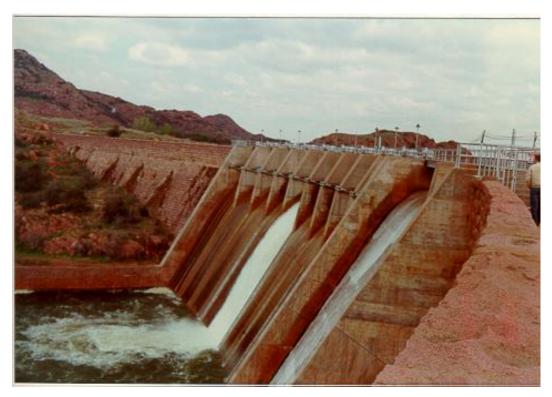


Figure 2 - Downstream Face of Altus Dam.

Incorporated near dam center are both controlled and uncontrolled overflow-type spillways. The uncontrolled section is 110.5 feet wide at crest elevation 1,559.0, with a discharge capacity of about 4,900 cubic-feet-seconds (cfs) at reservoir elevation 1,564.0. The controlled portion is regulated by nine radial gates, each 21 feet wide and 15 feet high. The controlled section is 229 feet wide at crest elevation 1,547.0 with a top of gate elevation of 1,562.0. The capacity of each radial gate at reservoir elevation 1,564.0 is about 5,800 cfs.

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<sup>&</sup>lt;sup>2</sup> The definition of such terms as "hydraulic height," "structural height," etc. may be found in manuals such as Reclamation's *Design of Small Dams* and *Guide for Preparation of Standing Operating Procedures for Dams and Reservoirs*, or ASCE's *Nomenclature for Hydraulics*.

The canal outlet works consists of three 72-inch diameter outlet conduits controlled by 5-foot by 5-foot high pressure gates. The canal outlet has a total capacity of 1,000 cfs at elevation 1,524.0 and 3,500 cfs at elevation 1,559.0. The original river outlet works through the dam are no longer operational.

The drainage area above the dam is 2,515 square miles of which 399 is considered noncontributing by the USGS. The area originates about 15 miles west of Amarillo, Texas and extends eastward into western Oklahoma. There are no known major structures in the watershed to reduce sediment contributions into the reservoir. However, the Granite Bridge and the State Highway 9 causeway, located within the reservoir about 9 miles upstream of the dam, have a dramatic affect on the sediment distribution within the reservoir. The Granite Bridge, near the east bank, is the only bypass for sediment downstream of the one-mile long causeway. The causeway is an elevated earthen dike that blocks about ninety percent of the reservoir. The 1970's developed USGS quad of the reservoir shows the North Fork Red River meandering upstream of the causeway from reservoir east bank to west bank, then running parallel along the causeway before entering the main body of the reservoir under the bridge. Since this 1970's developed map, the route of the river upstream of the bridge has straightened out where it now runs along the east bank of the reservoir. The reservoir is around 13.1 miles long with an average width of one mile (Figure 3).

Reservoir sedimentation is an ongoing depositional process that can remain invisible for a significant portion of the life of a reservoir. As the river enters the reservoir the flow depth increases and velocity decreases, resulting in a loss in the sediment transport capacity of the inflow, and allowing the sediment to deposit in the upper reservoir area (Figure 4). Initially the sediment deposition process occurred somewhat differently in Altus Reservoir. The Granite Bridge causeway in Altus Reservoir acted as a dam, meaning the majority of the inflowing sediment initially deposited in the very upper operation elevation range of the reservoir above this structure. The 1948 and 1967 surveys measured the most significant change due to sediment deposition in the reservoir above the causeway (Lara, 1971). As early as the 1967 reservoir survey, a drawdown of only a few feet resulted in a large exposure of the lake bottom in the upper reservoir area where the majority of the initial sediment had been deposited. With so much of the original upper area having been filled with sediment during the early years of reservoir operations, and with the river now flowing more directly into the main reservoir area below the causeway, the majority of future inflowing sediments will be deposited in the main body of the reservoir downstream of the bridge.

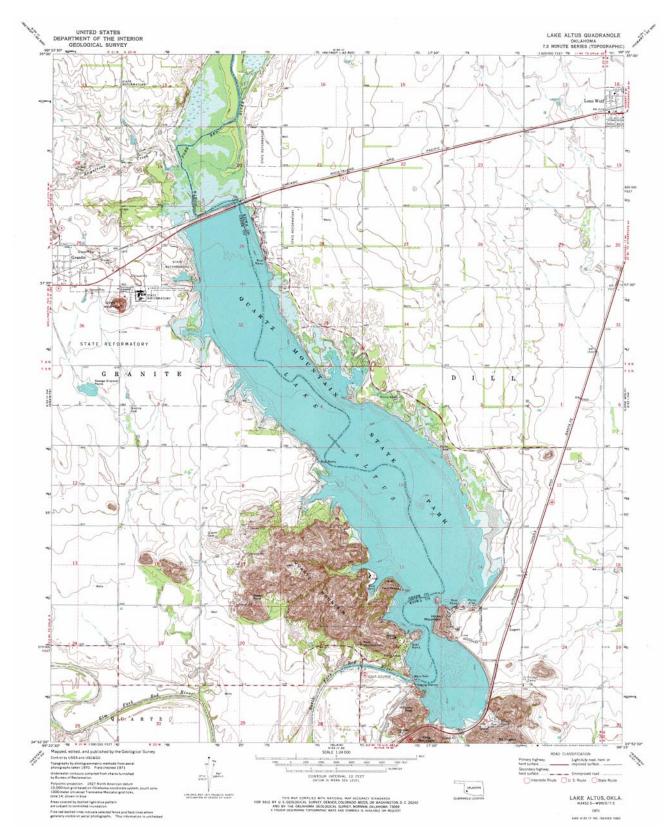


Figure 3 - USGS Quad of Altus Reservoir

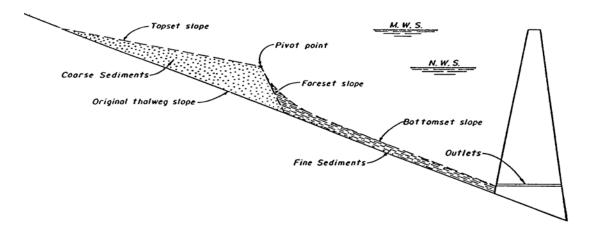


Figure 4 - Reservoir Sediment Delta Formation.

# **Summary and Conclusions**

This Reclamation report presents the results of the 2007 survey of Altus Reservoir. The primary objectives of the survey were to gather data needed to:

- develop reservoir topography
- compute area-capacity relationships
- estimate storage depletion, by sediment deposition, since dam closure

A control survey was conducted using the on-line positioning user service (OPUS) and RTK GPS to establish a horizontal and vertical control network near the reservoir for the hydrographic surveys. OPUS is operated by the National Geodetic Survey (NGS) and allows users to submit GPS data files that are processed with known point data to determine positions relative to the national control network. Initially, the GPS base was set over a temporary rebar on East Dike. The coordinates for this point were processed using OPUS, and from this base additional points were established and checked during the November 2006 and February 2008 land surveys and the June 2007 bathymetric surveys.

The horizontal control for this study was in feet, Oklahoma South state plane coordinates, in the North American Datum of 1983 (NAD83). The vertical control was in feet, tied to NAVD88 and the Reclamation project vertical datum. All elevations in this report are referenced to Reclamation's project or construction vertical datum that is near NGVD29 and about 0.5 feet lower than NAVD88.

In November 2006, the RTK GPS land survey was conducted near reservoir elevation 1,541. Since the basin had been dry for several years, the survey was conducted assuming the data would be combined with a spring 2007 bathymetric survey where the inflows would provide overlap between the two surveyed areas.

With the high 2007 spring inflows, the reservoir filled and was near elevation 1,559 when the underwater survey was conducted in June 2007. The bathymetric survey used sonic depth recording equipment interfaced with RTK GPS for determining the sounding locations. The system continuously recorded depth and horizontal coordinates of the survey boat as it navigated along grid lines covering Altus Reservoir. The collection system also provided information to allow the boat operator to maintain a course along these grid lines. The water surface elevations recorded by Reclamation's reservoir gage during the time of collection were used to convert the sonic depth measurements to reservoir bottom elevations. The initial above-water topography was determined by digitizing contour lines from the USGS quads of the reservoir area. The November 2006, June 2007, and February 2008 data was used to make adjustments to the initial digitized contours due to some shoreline erosion and changes in the upper reservoir resulting from sediment delta formation.

In February 2008, a four-day RTK GPS land survey was conducted near reservoir elevation 1,553. The survey covered a small portion of the shoreline in the main body of the reservoir and areas above the causeway. The shoreline data was compared with the USGS quad contours and where the survey indicated changes, the quad contours were adjusted for new map development. The 2006 and 2007 surveys were not able to obtain access above the causeway due to the extensive vegetation that had developed over the years while the reservoir was drawdown during the extended draught. After the reservoir filled in 2007, this vegetation was flooded causing much of it to die off. The February survey was able to gain access and RTK GPS collection in some of the open areas of the reservoir where defoliation had occurred due to the die off and cold temperatures during the winter months. There were still vast areas of the upper reservoir and along the shoreline where access was not possible due to the remaining dense vegetation and debris. The only means to obtain enough data to accurately map these areas would be aerial collection. A combination of mapping experience, engineering judgment, land survey data, and USGS quad contours, were used to develop the new upper reservoir topography.

The new 2007 Altus Reservoir topographic map is a combination of the adjusted digitized quad contours, 2006/2008 land survey data and the 2007 underwater survey data points. A topographic computer program generated the 2007 reservoir surface areas at predetermined contour intervals from the combined reservoir data. The 2007 area and capacity tables were produced by a computer program that used the measured contour surface areas and a curve-fitting technique to compute the area and capacity values at prescribed elevation increments (Bureau of Reclamation, 1985).

Tables 1 and 2 contain summaries of Altus Reservoir and watershed characteristics for the 2007 study. The 2007 survey determined the reservoir has a total storage capacity of 162,526 acre-feet with a surface area of 7,170 acres at the top of the surcharge pool, elevation 1,564.0. Since December 1940 dam

closure, the reservoir has an estimated volume change of 30,316 acre-feet below elevation 1,564.0 and 27,749 acre-feet below top of conservation elevation 1,559.0, resulting in a 17.7 percent loss in original capacity below elevation 1,559.0. This equates to an average annual loss of 417 acre-feet between 1940 and 2007.

# **Control Survey Data Information**

Prior to the surveys, a temporary point was set on East Dike using OPUS to establish the horizontal and vertical control datum (Figure 5). OPUS is operated by the NGS and allows users to submit GPS data files that are processed with known data to determine point positions relative to the national control network. The East Dike temporary point was used as the base for the November 2006, June 2007, and February 2008 surveys.



Figure 5 - Temporary Point set on East Dike, November 2006.

The horizontal control was in Oklahoma south zone state plane coordinates in NAD83 and the vertical control was tied to NAVD88 and the Reclamation project vertical datum. All elevations in this report are referenced to Reclamation's project or construction vertical datum that is near NGVD29 and around 0.5 feet lower than NAVD88. During the November 2006 survey a control shot was taken on a brass cap located along the dam alignment on the right bank with following results:

North 568,239.44 East 1,579,523.30 Elevation 1,570.34

The Oklahoma-Texas Area Office forwarded control data information for a brass cap, labeled F105 with following coordinates in NAD27 and NGVD29:

North 568,201.67 East 161,122.26 Elevation 1,569.65

The point data information was converted to NAD83 and NAVD88 using the Corp of Engineers conversion program CORPSCON:

North 568,241.30 East 1,579,523.24 Elevation 1,570.18

It appears from the coordinates that they are the same datum point. The difference vertically is very small, only 0.16 feet, but there is a two-foot horizontal shift. This point was shot from a temporary base station established in the upper reservoir area. The brass cap was unmarked and visually worn. The information could be used as a control check during future surveys.

# **Reservoir Operations**

Altus Reservoir is part of the W.C. Austin Project that was designed to provide storage for irrigation, municipal water, and flood control. The project also provides benefits for fish and wildlife conservation and recreation facilities. The June 2007 capacity table lists 162,526 acre-feet of total storage below the maximum water surface elevation 1,564.0³, table 1. The 2007 survey measured a minimum lake bottom elevation of 1,510.5. The following values are from the June 2007 capacity table:

- 13,981 acre-feet of surcharge pool storage between elevation 1,562.0 and 1,564.0
- 19,626 acre-feet of flood control pool storage between elevation 1,559.0 and 1,562.0
- 128,286 acre-feet of conservation pool storage between elevation 1,517.5 and 1,559.0
- 633 acre-feet of dead pool storage below elevation 1,517.5.0

<sup>3</sup> 2007 Altus Reservoir area and capacity tables were extended to elevation 1,570.0. From elevation 1,564.0 through 1,566.67, top of parapet wall, there is 19,903 acre-feet of storage.

The computed annual inflow and reservoir stage records for Altus Reservoir are listed by water year in Table 1 for the available period 1945 through 2007. The inflow values were computed by the Great Plains Regional Office and showed the annual fluctuation with a computed average annual inflow of 104,039 acre-feet. The maximum reservoir elevation of 1,562.1 was recorded during water year 1951. The minimum reservoir elevation of 1,523.0 was recorded during water year 1985. During water years 2002 through 2007, the reservoir was below elevation 1,530 four out of the six years of reservoir operation, meaning the active reservoir body remained between the dam and the Granite Bridge.

# Hydrographic Survey Equipment and Method

The hydrographic survey equipment was mounted in the cabin of a 24-foot trihull aluminum vessel equipped with twin in-board motors (Figure 6). The hydrographic system included a GPS receiver with a built-in radio, a depth sounder, a helmsman display for navigation, a computer, and hydrographic system software for collecting the underwater data. An on-board generator supplied power to all the equipment. The shore equipment included a second GPS receiver with an external radio. The GPS receiver and antenna were mounted on a survey tripod over a known datum point and a 12-volt battery provided the power for the shore unit.



Figure 6 - Survey Vessel with Mounted Instrumentation on Jackson Lake in Wyoming.

The Sedimentation and River Hydraulics Group uses RTK GPS with the major benefit being precise heights measured in real time to monitor water surface elevation changes. The basic output from a RTK receiver are precise 3-D coordinates in latitude, longitude, and height with accuracies on the order of 2 centimeters horizontally and 3 centimeters vertically. The output is on the GPS

datum of WGS-84 that the hydrographic collection software converted into Oklahoma's state plane coordinates, south zone in NAD83. The RTK GPS system employs two receivers that track the same satellites simultaneously just like with differential GPS.

The Altus Reservoir bathymetric survey was conducted from June 4 through June 9 of 2007 between water surface elevation 1,559.2 and 1,559.5 (Reclamation project datum). The boat was not used for several of the days due to extreme winds. The bathymetric survey was conducted using sonic depth recording equipment, interfaced with a RTK GPS, capable of determining sounding locations within the reservoir. The survey system software continuously recorded reservoir depths and horizontal coordinates as the survey boat moved along closely spaced grid lines covering the reservoir area. Most transects (grid lines) were run somewhat parallel to the upstream-downstream alignment of the reservoir at around 200-foot spacing. The survey vessel's guidance system gave directions to the boat operator to assist in maintaining the course along these predetermined lines. Data was collected along the shore by the survey vessel for the majority of the reservoir. There were coves on both the east and west sides of the reservoir that were not covered by the survey vessel due to shallow water conditions and thick vegetation that invaded those areas during the recent reservoir draw down. Vegetation was also a problem in the very upper reach of the reservoir, both upstream and downstream of the Granite Bridge where it hindered access by the survey vessel. During each run, the depth and position data were recorded on the laptop computer hard drive for subsequent processing. Final processing of the underwater collected data set resulted in around 98,000 points (Figure 7).

The 2007 underwater data was collected by a depth sounder calibrated by lowering an instrument that measured the sound velocity of the reservoir water column. The individual depth soundings were adjusted by the speed of sound of the measurements which can vary with density, salinity, temperature, turbidity, and other conditions. The soundings were further verified by lowering a weighted cable below the boat with beads marking known depths. The collected data were digitally transmitted to the computer collection system through a RS-232 port. The depth sounder also produced an analog hard-copy chart of the measured depths. These graphed analog charts were analyzed during post-processing, and when the analog charted depths indicated a difference from the computer recorded bottom depths, the computer data files were modified. The water surface elevations at the dam, recorded by a Reclamation gage, were used to convert the sonic depth measurements to true lake-bottom elevations. Additional information on collection and analysis procedures is included in *Engineer and Design*: Hydrographic Surveying (Corps of Engineers, January 2002) and Reservoir Survey and Data Analysis (Ferrari and Collins, 2006).

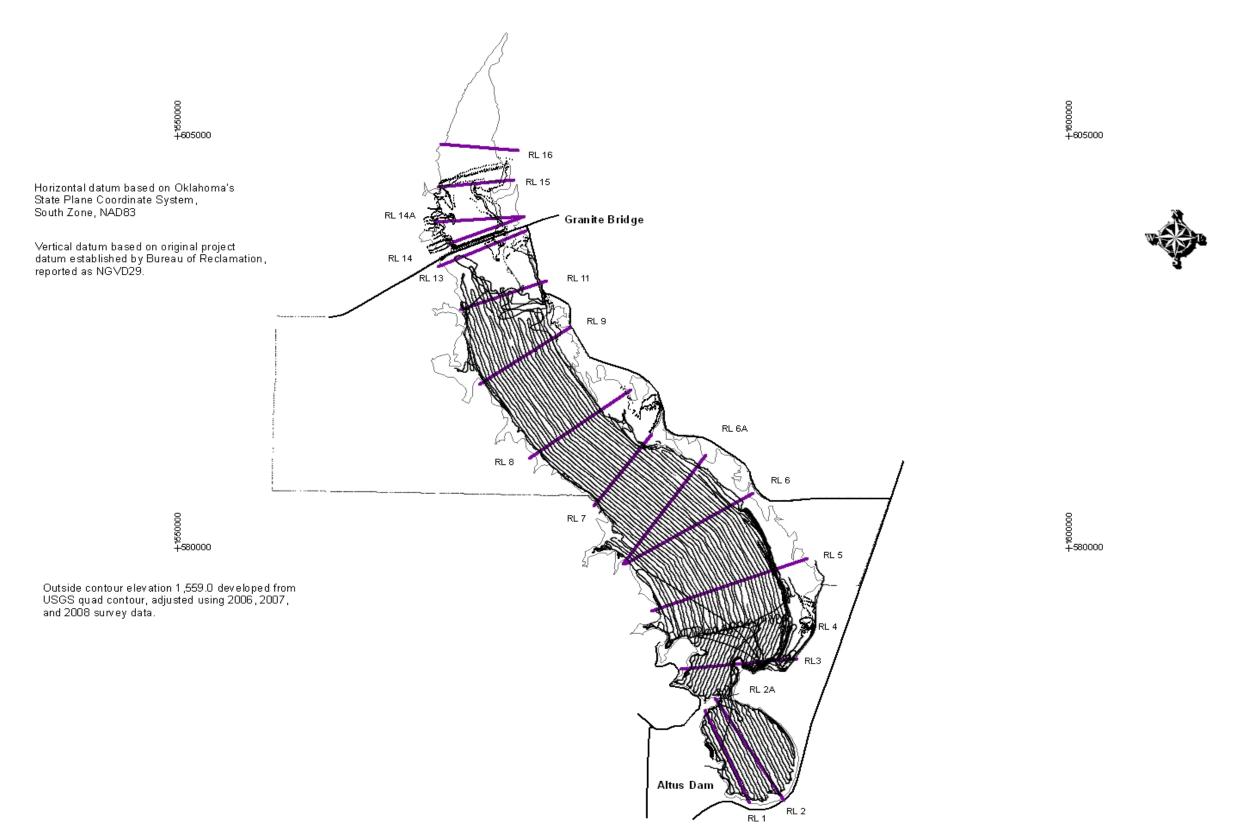


Figure 7 - Altus Reservoir 2006/2007/2008 survey data points.

A RTK GPS land survey was conducted by personnel from Reclamation and Lugert-Altus Irrigation District in November 2006 when the reservoir level was low, near elevation 1,541. Due to the extended drought and calls to survey the reservoir, the land survey was conducted under the assumption that the reservoir may not rise very much during spring runoff. Under that assumption, the land survey concentrated within the lower reservoir elevations where the terrain was wide open and sediment deposition had occurred. The survey was accomplished by mounting the RTK GPS receivers on all-terrain vehicles (ATV's) and setting them to automatically collect data every ten feet as the ATV's proceeded around the reservoir area where they had access (Figure 8). Access was limited due to thick vegetation in the upper elevations along the shore, upstream of the Granite Bridge, and also areas just downstream of the bridge. Collection near the existing water surface was also limited due to the soft bottom conditions that caused the vehicles to become stuck at times. Some data was collected on foot below the Granite Bridge along the river channel where openings in the vegetation allowed access and RTK GPS collection (Figure 9). The ground survey data was tied to the same control network as the bathymetric collection with elevations tied to NAVD88. During post processing, the elevations were shifted to match the Reclamation vertical datum, near NGVD29.



Figure 8 - RTK GPS instruments mounted on all terrain vehicles in upper reservoir area. Far vehicle is parked near the reservoir water's edge.



Figure 9 - View from the Granite Bridge looking upstream. Shows the thick vegetation that has established itself on the sediment deposition, preventing access for GPS measurements.

In February 2008, an additional RTK GPS land survey was conducted by personnel from Reclamation and the Lugert-Altus Irrigation District when the reservoir level was near elevation 1,553. The four-day survey was conducted along a small portion of the shoreline in the main body of the reservoir and above the causeway. The shoreline data was compared with previous digitized USGS quad contours that were adjusted as warranted. The previous surveys were not able to gain access above the causeway due to the extensive vegetation growth while the reservoir was drawn down over the past few years. Full reservoir operation in 2007 flooded and killed some of this vegetation. The February survey was able to gain access in some open areas of the reservoir where the defoliation allowed RTK GPS ground shots. There was still a vast portion of the reservoir in the upper area and along the shoreline where access and GPS collection was not possible due to the thick vegetation and debris, especially in the extreme upper reservoir above elevation 1,556. The only means to obtain enough data to accurately map these areas of the reservoir would be aerial collection. But the 2006 and 2008 land surveys did allow limited reservoir topographic development. During the February 2008 survey, there was a shallow body of water upstream of Granite Bridge similar to that shown in the photograph on the cover of this report and in Figure 33. At the time of the 2008 survey, there was no connecting channel between this body of water and the main reservoir. The survey measured the upper body water surface about one foot higher than the main body reservoir water surface. The two bodies connect near reservoir elevation 1555.

# Reservoir Area and Capacity

#### **Topography Development**

The topography of Altus Reservoir was developed from the 2006 and 2008 above water survey data, the 2007 below water survey data, and the digitized contours from the USGS quad maps. The USGS quad contours at elevations 1,547.0, 1,550.0 and 1,559.0 were developed from aerial photography dated 1970. The modified elevation 1,559.0 contour was used as a hard boundary for the 2007 developed contours, allowing contour mapping only within the reservoir area outlined by this hardclip contour. The 2006, 2007, and 2008 survey data sets were used to make adjustments to the initial digitized 1,559.0 contour where shoreline erosion and deposition occurred in the lower reservoir reach, but the majority of the adjustment was done in the upper reservoir above the causeway where the majority of the sediment deposition has occurred.

The adjusted contour, elevation 1,559.0, was used to perform the hardclip around the survey data points from elevation 1,559.0 and below within Altus Reservoir. The hardclip was used during the triangular irregular network (TIN) development to prevent interpolation outside the enclosed polygon. The 1,559.0 contour was selected for the hardclip boundary since it was the closest data available to represent the water surface during the 2007 underwater survey. There was adequate RTK GPS ground collection data near elevation 1,559.0 upstream and downstream of Granite Bridge to allow adjustments to be made to the USGS quad contour with confidence, but aerial collection would provide the most reliable method of mapping the above water topography.

Using ARC GIS editor, the 2006, 2007, and 2008 survey data sets along with all the digitized contours were plotted. There were coves on both the east and west sides of the reservoir and in the area upstream of Granite Bridge that were not covered by any of the surveys due to the thick vegetation that invaded these areas during recent years of reservoir draw down. This was also a problem in the very upper reach of the reservoir just downstream of the Granite Bridge where thick vegetation hindered access by the survey vessel during the underwater survey and prevented access during both land surveys. For these areas, data points were added for elevation 1,447.0; 1,550.0; 1,552.0; 1,554.0 and 1,559.0 using the quad map contours and limited survey data as a guide. In the cove areas of the reservoir, one would expect minimal change due to sediment inflow. However, the 2008 ground survey did measure some change. These measured changes were limited and were attributed to reservoir bank erosion and wind blown sediments.

Using Google Earth (http://earth.goggle.com) a satellite image of the reservoir was obtained from a period when the reservoir water extended above the Granite Bridge. It was assumed the reservoir water surface in the satellite image was near

elevation 1,555.0 or slightly higher. The satellite image showed the reservoir water body in the coves similar in shape to the upper USGS quad contours. Using all available information, points were added along the elevation 1,547.0 and 1,550.0 quad contours in the side coves as necessary to allow the software program to develop more accurate contours. The cross sections collected during the 1967 Altus Reservoir survey showed that much of the original area upstream of Granite Bridge, above elevation 1,550.0, had been lost due to sediment deposition. Additional confirmation of this deposition was obtained from the 2008 land survey. Points were also added along the upstream causeway alignment and pond outline. The points were added using ARCGIS editor where they were interpolated using all available data and previous mapping experience.

Contours for the reservoir below elevation 1,559.0 were developed from the TIN generated within ARCGIS. A TIN is a set of adjacent non-overlapping triangles computed from irregularly spaced points with x,y coordinates and z values. A TIN is designed to deal with continuous data such as elevations. The TIN software uses a method known as Delaunay's criteria for triangulation where triangles are formed among all data points within the polygon clip. The method requires that a circle drawn through the three nodes of a triangle will contain no other point, meaning that all the data points are connected to their nearest neighbors to form triangles. This method preserves all the collected data points. The TIN method is discussed in detail in the ARCGIS user's documentation, (ESRI, 2007).

The linear interpolation option of the ARCGIS TIN and CONTOUR commands was used to interpolate contours from the Altus Reservoir TIN. The areas of the enclosed contour polygons at one-foot increments were computed from the survey data for elevations 1,511.0 through 1,556.0. Since limited above water data was collected, this study assumed no change in reservoir surface area since the 1967 survey at elevation 1,565.0 and higher. The surface area of the developed elevation 1559.0 contour, minus the island areas, was used for the 2007 area and capacity computations. The reservoir contour topography at 2-foot intervals from elevation 1,556.0 and below is presented on Figure 10. Development of the contours within ARCGIS was directly from the TIN using all the enclosed data points resulted in a somewhat jagged representation of the contours. There are other mapping packages that can be used to generate smoother contours, but for this study the TIN approach including all data points was used to produce the most accurate surface area and resulting volume. The best means to develop the upper contours and resulting above water reservoir areas would be by aerial survey with the reservoir drawn down, but budget limitations prevented such collection.

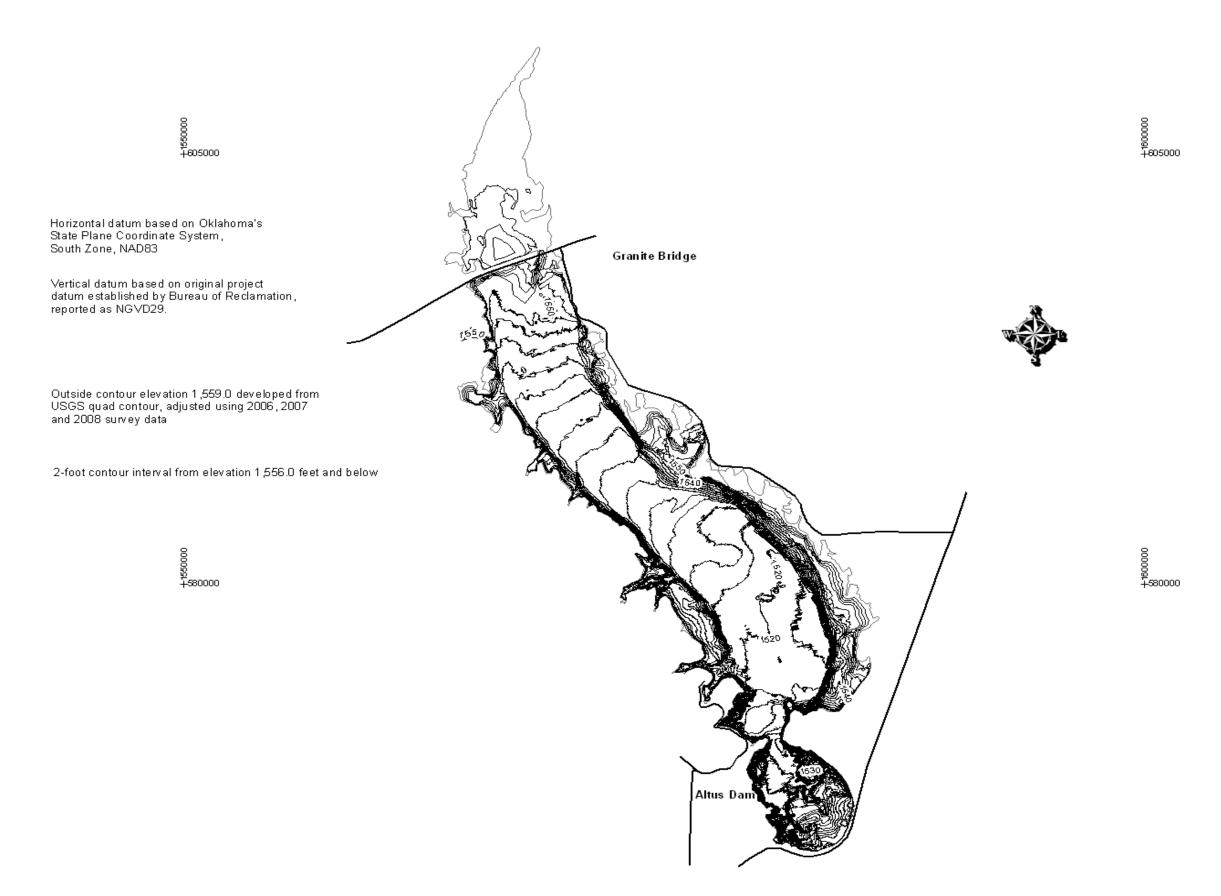


Figure 10 - Altus Reservoir topographic map.

#### **Lateral Distribution**

Profiles of several of the 25 previously surveyed sedimentation range lines were developed during this study to provide a visual representation of the lateral sediment deposition change since the 1948 and 1967 surveys (Figures 11 through 26). The location of the range lines along with the data points collected by this study are presented on Figure 7. The range line locations were visually determined from the reservoir sedimentation range system maps presented in the 1967 survey report. The range line plots were recreated by digitizing the 1948 and 1967 sedimentation range plots presented in the 1967 report (Lara, 1971). It appears the plots are from left to right bank looking downstream. The plots in the 1967 report were of a small scale, but enough detail was presented to allow digital interpolation. Using tools within ARCGIS, 2007 cross section data was developed by cutting profiles through the surveyed data points. The routine stored the nearest points along the projected range lines. These stored points varied from 10 to 50 feet from the projected alignment depending on available data. As seen from Figure 7, there were no data points from Range Lines 16 and above, and only limited data points available for Range Lines 13, 14, and 14a. Thick vegetation would have hindered much of the data collection above range line 16, but previous survey results showed that this area of the reservoir had mostly silted in laterally from elevation 1,555.0 and below. The 1967 results showed that large areas above elevation 1,559.0 had also been lost to sediment deposition.

The Range Line plots provided valuable insight into the change in lateral sediment distribution. Range Lines 1 and 2 showed minimal sediment deposit since 1967 considering the length of time (40 years) between surveys. Minor sediment deposition was also measured at Range Lines 2A, 3, 4, 5, 6, 6A, 7 and 8. The first significant lateral buildup of sediment occurred at range line 9, located about 1.5 miles downstream of the causeway. Considerable sediment buildup was also measured at Range Lines 11 and 13, located downstream of the causeway. At Range Line 14, located just upstream of the bridge and causeway, there has been about five feet of sediment deposition since the 1967 survey. Even though limited 2008 survey data was collected above the causeway, the developed Range Lines 14, 14A, and 15 each showed the sediment level near elevation 1,555. Range Lines 14 and 14A cross the existing upstream water pond, but it appeared the average depth was only a few feet and would not significantly impact the average bottom elevation computations at these locations. Range Lines 14A and 15 showed a minimal change in the top sediment level since the 1967 survey. It was assumed that surveys of Range Line 16 and above would have produced similar general results.

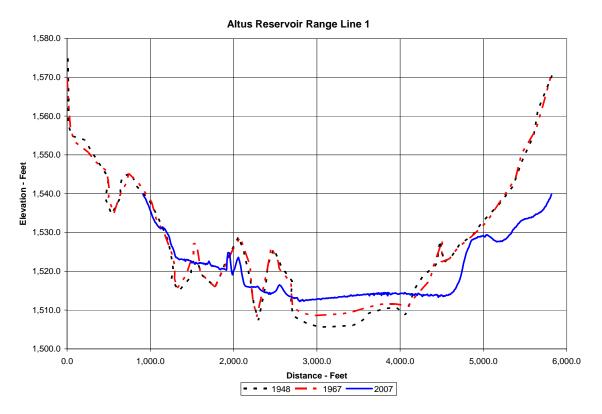


Figure 11 - Range Line 1.

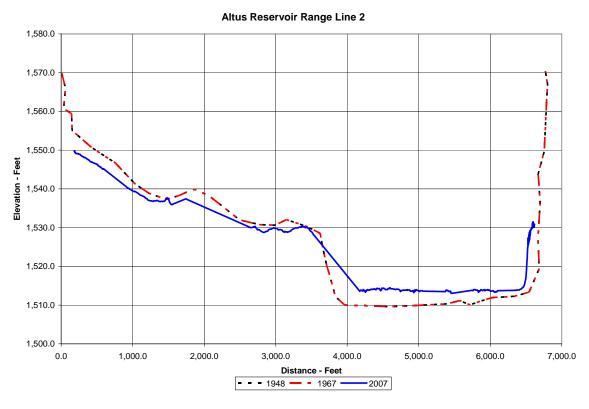


Figure 12 - Range Line 2.

#### Altus Reservoir Range Line 2A

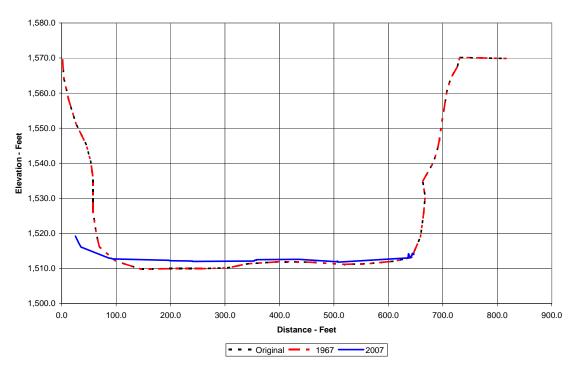


Figure 13 - Range Line 2A.

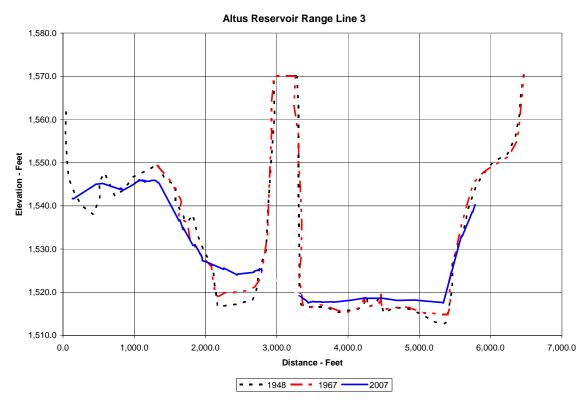


Figure 14 - Range Line 3.

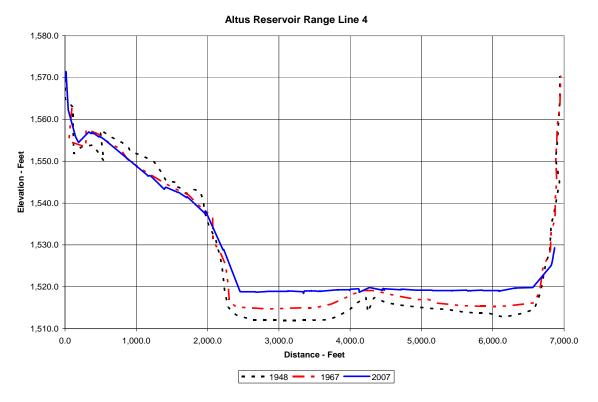


Figure 15 - Range Line 4.

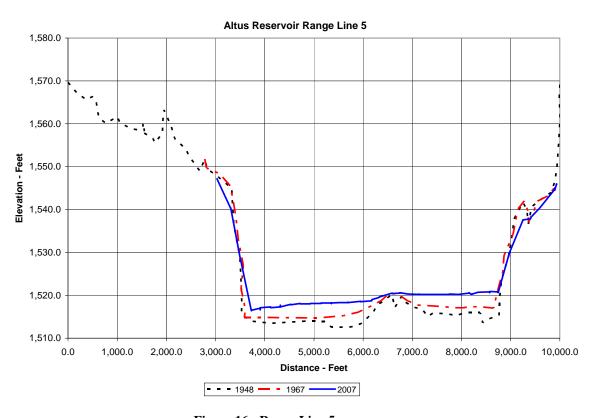


Figure 16 - Range Line 5.

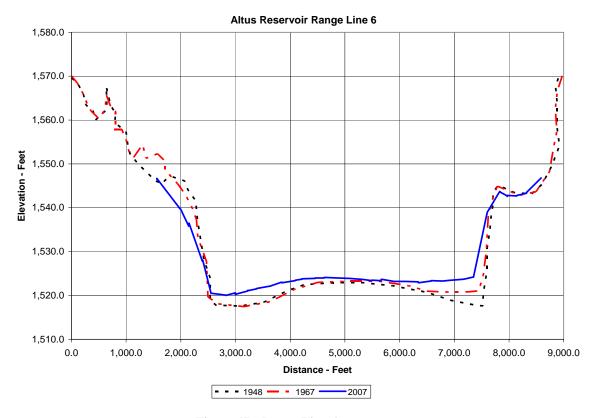


Figure 17 - Range Line 6.

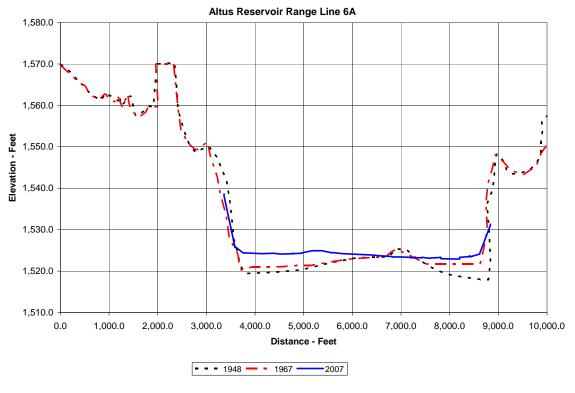


Figure 18 - Range Line 6A.

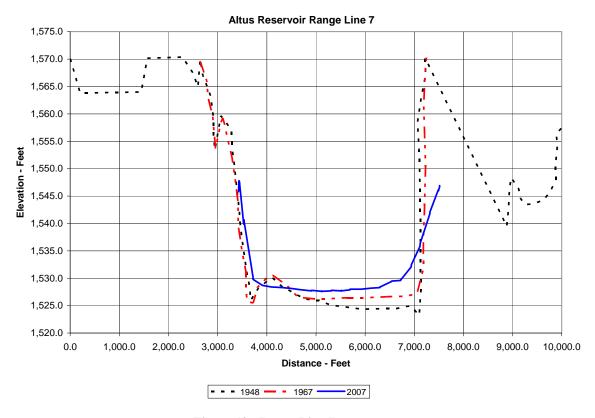


Figure 19 - Range Line 7.

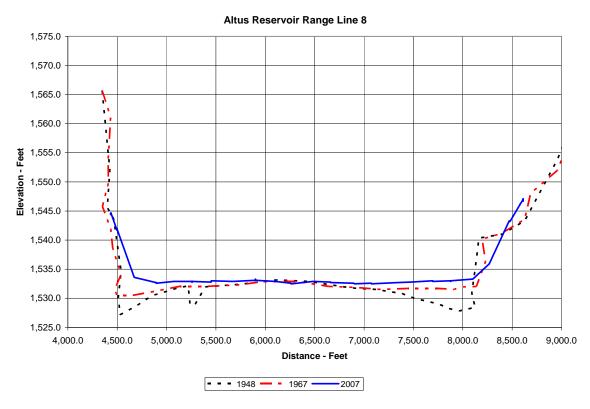


Figure 20 - Range Line 8.

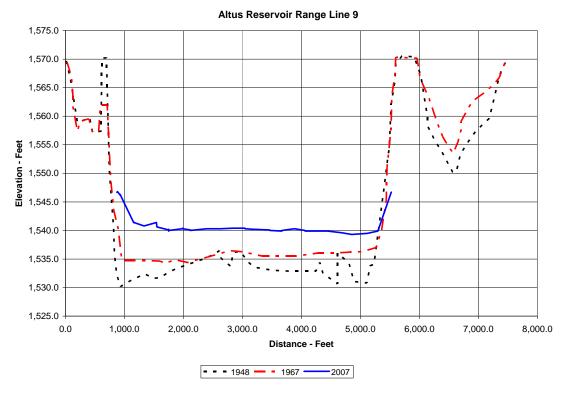


Figure 21 - Range Line 9.

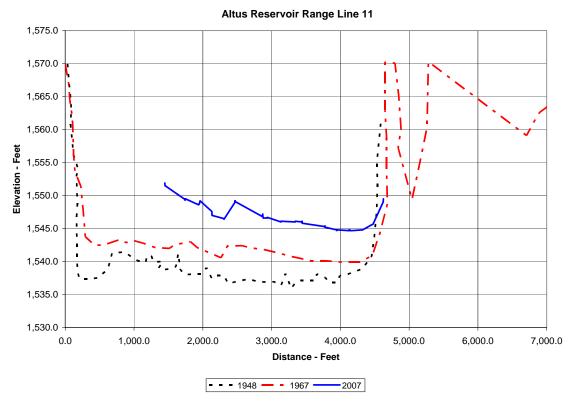


Figure 22 - Range Line 11.

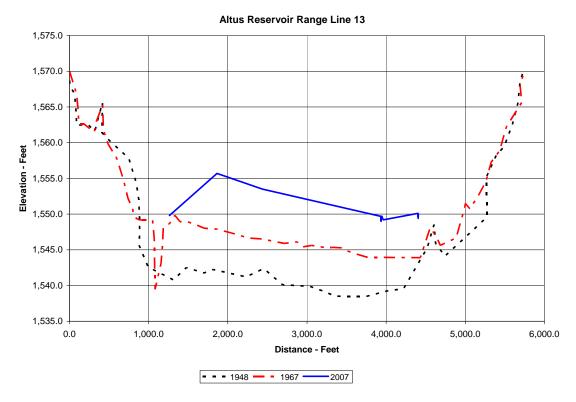


Figure 23 - Range Line 13.

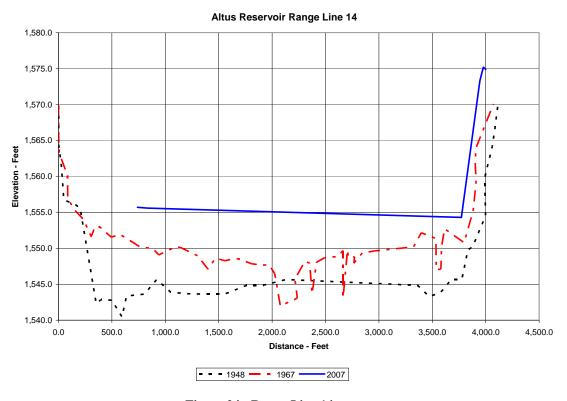


Figure 24 - Range Line 14.

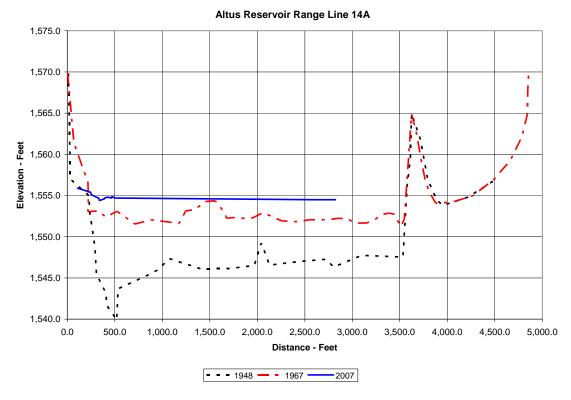


Figure 25 - Range Line 14A.

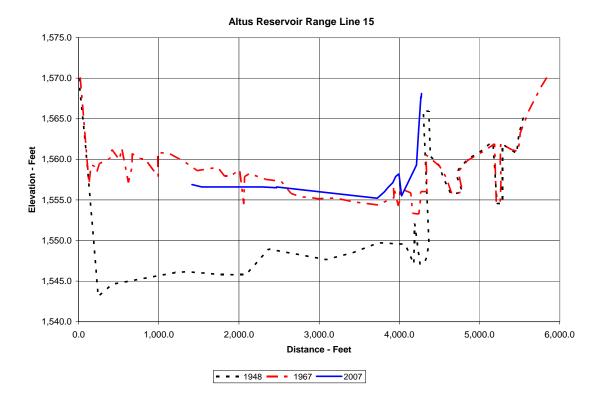


Figure 26 - Range Line 15.

#### **Longitudinal Distribution**

A means to further illustrate the sediment accumulation is a longitudinal plot of the distribution throughout the reservoir from Range Line 1 upstream (Figure 27). The longitudinal profile of the original river channel was projected from a small plot presented in the 1967 report. The profiles from 1948, 1967 and 2007, for Range Lines 1 through 15, were developed by computing the average main channel bottom elevation for each range line. To extend the 1948 and 1967 profiles above Range Line 15, the location and elevations were interpolated from the plot in the 1967 report. The profile shows an extreme rise in sediment depths occurring at Range Line 14, located just upstream of the Granite Bridge. From this pivot point (Figure 4), the sediment deposition slopes upstream, but does not show a major change since the 1967 survey. It is assumed that the 2007 profile upstream of Range Line 15 would not differ much from the 1967 profile. The rise of sediment depth at Range Line 14 going upstream for both the 1967 and 2007 surveys shows the influence of the causeway that restricts the inflowing river sediment before it enters the main reservoir body by passing downstream under the bridge. The 2007 plot shows the sediment build up downstream of the bridge (foreset slope) at Range Lines 9, 11 and 13. Further downstream towards the dam (Range Line 8 downstream), the sediment deposited along the bottomset slope to the dam and only shows a slight build up since the 1967 survey. Over time, it is expected the pivot point will begin to move further downstream, but the causeway will continue to influence this along with the sediment inflow rate. The comparison of the 1948, 1967 and 2007 profiles illustrates that the sediment inflow into the reservoir as been significantly reduced since the 1967 survey. The depths between these profiles show the buildup between the survey periods with the 2007 profile only showing a major change from Range Line 9 upstream to Range Line 14. When you figure the time period between the surveys, the profiles further illustrate the significant reduction in sediment inflow since the 1948 and 1967 surveys.

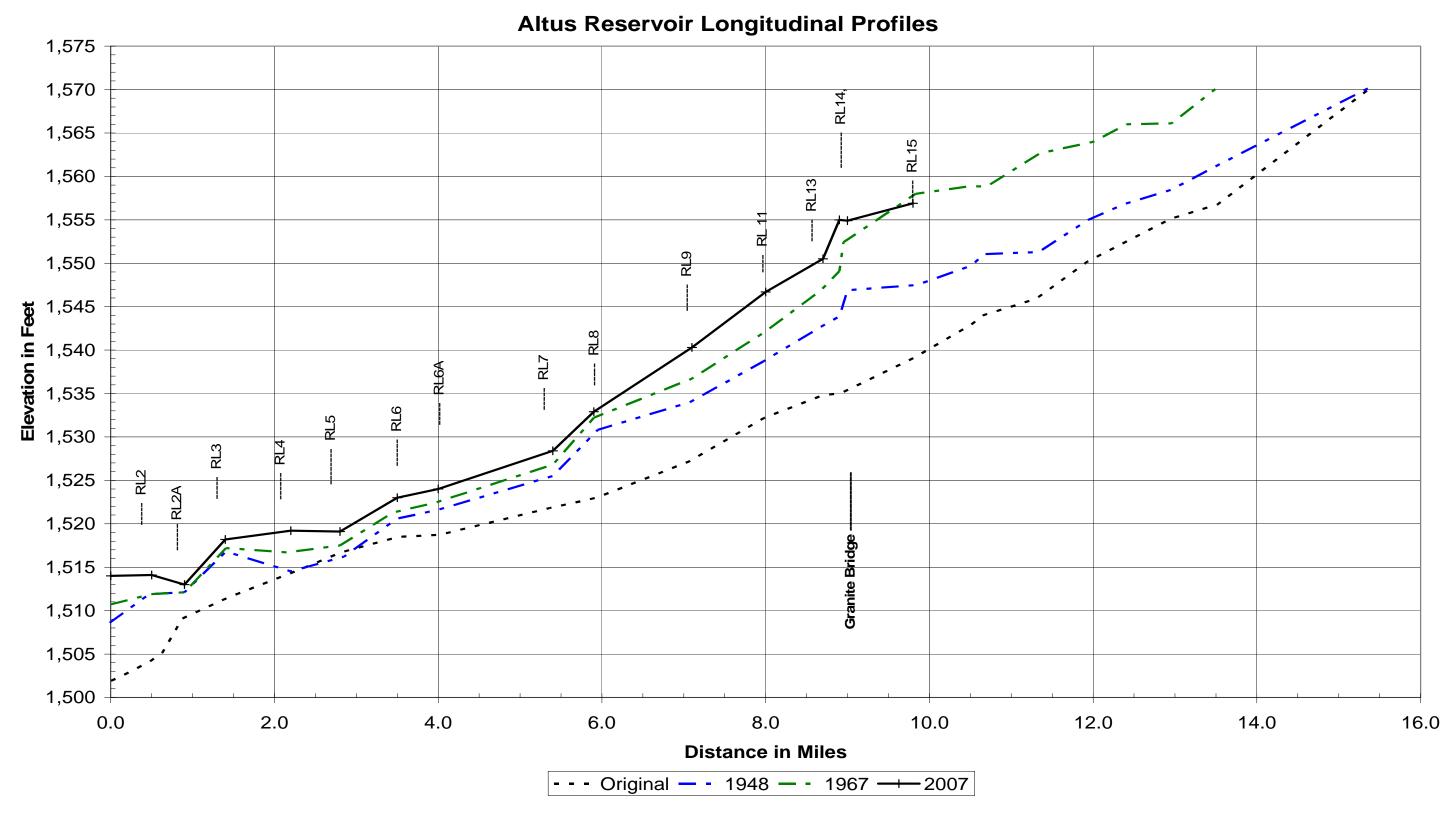


Figure 27 - Altus Reservoir longitudinal profile.

# **Development of the 2007 Altus Reservoir Surface Areas**

The 2007 surface areas for Altus Reservoir were computed at 1-foot increments directly from the reservoir TIN from elevation 1,510.0 through 1,556.0. The TIN was developed from collected and interpolated data sets within the hardclip polygon created from the previously described digitized 1,559.0 contour. Surface area calculations were performed using ARCGIS commands that compute areas at user-specified elevations directly from the TIN. For the purpose of this study, the measured survey areas at 2- and 5-foot increments from elevation 1,510.0 through 1,556.0 were used in computing the new area and capacity tables. The 2007 adjusted 1,559.0 contour with resulting surface area was an input for computing the new area and capacity tables. This study assumed no change in surface area, since the 1967 survey, at elevation 1,565.0 and above. A straight line interpolation was used to compute the surface areas between elevations 1,559.0 and 1,565.0. A 1967 area and capacity table was located that showed the 1967 study computed the surface area and resulting capacity using straight-line interpolation between elevation 1,550.0 to 1,565.0. No written explanation was given, but the 1967 Altus Reservoir study did have surveyed range lines in the upper reservoir that measured the major changes.

The 1967 surveyed cross sections above the Granite Bridge showed the causeway as a major restriction of sediment flowing into the lower body of the reservoir. The 1967 cross sections showed that since the 1948 survey, the majority of the surface area from the causeway upstream from elevation 1,550.0 and below had been lost due to sediment accumulation. The surveyed range lines also showed that a large portion of the surface area above elevation 1,550.0 had been lost due to sediment deposition. Due to this measured deposition, it appears the 1967 method of projecting the data between elevations 1,550.0 to 1,565.0 was the only means available outside of additional data collection. The 2007 study had the same issues, but the collected data determined that projecting was only necessary from elevation 1,559.0 to 1,565.0.

Table 1 provides a summary of all the surveys that have been conducted on Altus Reservoir including the 1940 (original), 1948, 1953, 1967, and 2007 results. The area and capacity curves for all of these surveys are plotted on Figure 28. The table and plots show interesting results from all of these surveys. The 1948 results actually showed a slight increase in surface area at elevation 1,559.0 while the 1953 and 1967 survey results showed a significant loss of surface area at the same elevation. The original surface areas were measured from developed contours, and until 2007, all the surveys were conducted by measuring 25 or 26 cross sections to represent the 16 mile length of Altus Reservoir. The 1967 Altus Reservoir surface areas were computed using the range width ratio method explained in more detail in Chapter 9 of the Sedimentation Groups Erosion and Sedimentation Manual (Ferrari and Collins, 2006).

At first look, one could question such a large loss of surface area at the elevation 1,559.0 contour in 1967 when compared to the previous surveys. Upon viewing the range line plots above the Granite Bridge, it showed that a major surface area loss occurred in these upper elevation contours (Figures 11 through 26 and Figures 29 through 32). The Figure 29 through 32 plots are of the 1948 and 1967 survey results showing the sediment build-up along these range lines.

As part of the 2007 analysis, the USGS quad contours of the reservoir area were digitized. These contours were developed from 1970 aerial photographs that were taken only three years after the 1967 survey. The following table shows the surface area results from the digitized contours along with the 1940 original and 1967 survey results.

<b>Elevation</b>	Year of Survey
(Feet)	(Surface area in acres)

	<u>1940</u>	<u>1967</u>	<u>1970 Aerial</u>
1,540.0	3,720	3,219	3,512
1,547.0	4,777	4,081	4,511
1,559.0	6,772	6,260	6,431

Note: For elevation 1,559.0, the total digitized USGS area is with the islands removed, but above the Granite Bridge there appears to be additional islands that show as high green shaded areas on the quad sheet.

The table results show the differences between using the range line method of computation, as was used in 1967, versus the 1970 aerial results. The 1970 surface areas for elevation 1,540.0 and 1,547.0 are both around ten percent higher than the 1967 results. For elevation 1,559.0, the difference was only three percent. There are errors associated with the scale of the USGS quad maps that need to be considered. But the aerial data should provide the most accurate measurement of the surface area throughout the reservoir. The aerial data included the shoreline coves that may have been projected as silted-in during the 1967 analysis. If the coves were improperly evaluated in 1967, some of the 1967 data results could be flawed. The 2007 study used the USGS quad contour data information to represent the side coves. The February 2008 RTK GPS survey helped in developing the elevation 1,559.0 contour that was used for the 2007 reservoir mapping. This additional data helped to validate the 1,559.0 contour development, but primarily assisted in adjusting this contour above the causeway that has been greatly affected due to sediment deposition. The computed surface area for the 2007 adjusted 1,559.0 contour was 6,273 acres, nearly matching the computed results projected during the 1967 surface area development.

# Altus Reservoir NAME OF RESERVOIR

 $\underline{\underline{1}}$  data sheet no.

7										DATA SHEET NO.			
D	1. O	WNER Bure	au of Recla	mation		2. STREAM	N	North Fork, Red Ri	3. STATE Oklahoma				
Α	4. SI	EC 22	TWP.	5N RA	NGE 20W	5. NEAREST	ГР.О. А	Altus	6. COUNTY Greer-Kiowa				
M	7. L	AT 34 °	53 ' 8	8 " LONG	99 ° 17 ' 43 "	8. TOP OF D	8. TOP OF DAM ELEVATION			9. SPILLWA	Y CREST EL	1559.0 <sup>3</sup>	
R	10.	STORAGE	1	1 ELEVATIO	N 12. ORIGINAL		13. ORI	GINAL	14. GROS	S STORAGE	15 DATE		
Е	ALL	OCATION	Т	TOP OF POOL	SURFACE ARI	EA, AC-FT	CAPACIT	ΓY, AC-FT	ACRE-FEET		STORAGE	3	
S	a.	SURCHARG	E	1,564.0		7,705		36,174		192,842	BEGAN		
Е	b.	FLOOD CON	TROL			,			1		_		
R	c	IRRIGATION		1,559.0		6,772		152,060		156,668	12/	1940	
V	d.	JOINT USE		1,000.0		0,772		102,000		120,000	16 DATE N	NORMAL	
o	e.	CONSERVA	TION						<del> </del>		OPERATION		
I	f.	INACTIVE	HOIV								BEGAN	0115	
R	σ.	DEAD	-	1,517.5		1,073	<u> </u>	4,608		4,608	— BEGAIN		
1	g. 17.	LENGTH OF R	ECEDVOID	13.1	MILES	AVG. WIDTI	T OE DECE		1	MILES	6/1	9/1946	
D					SOUARE MILES				24.			DICHEC	
В	18.	TOTAL DRAIN						PRECIPITATION				INCHES	
A	19.	NET SEDIMEN				QUARE MILE		MEAN ANNUAL		0.9		INCHES	
S	20.	LENGTH	146.5 MII			MILES 24.		NNUAL INFLOW		04,039 8		CRE-FEET	
I	21.	MAX. ELEV.	ATION		ELEVATION	25.	ANNUAL	L TEMP, MEAN	63 °F	RANGE -	-11 °F to 1	20 °F <sup>7</sup>	
N		3,500+		1496.7									
		DATE OF	27.	28.	29. TYPE OF	30. NO. OF	3	1. SURFACE	32.	CAPACITY	33. C/	/	
S	SUR	VEY	PER.	PER.	SURVEY	RANGES OR	R A	AREA, AC.	ACRE	- FEET	RATIO	AF/AF	
U	L		YRS	YRS	<u> </u>	INTERVALS							
R		12/1940			Contour (D)	2 to 5-f	eet	6,772		156,668	1	.51	
V		6/1948	7.5	7.5	Range (D)	26		6,793		148,640	1	.43	
Е		7/1953	5.1	12.6	Range (D)	25		6,575		142,862		.37	
Y		4/1967	13.8	26.4	Range (D)	25		6,260		134,494		.29	
		6/2007	40.1	66.5	Contour (D)	2-ft	9	6,273		128,919		.24	
	26.	DATE OF	34. PER			ATER INFLOW				TER INFLOW			
D		VEY	ANNUAL										
A			PRECIPIT		a. MEAN ANN.	b. MAX. AN	N. c	. TOTAL	a. ME	AN ANN.	b. TOT.	AL	
Т		6/1948	TRECTI	27 10	126,980	256.7	700 <sup>10</sup>	952,3	320	126,9	980	952,320	
A		6/1953		20.3 10	107,940		400 <sup>10</sup>	550,473		119,2		1,502,793	
A		4/1967		20.3 24.4 <sup>10</sup>	89,000	100 0	300 <sup>10</sup>			103,4			
		6/2007		24.4	95,356 <sup>8</sup>			1,227,897 3,823,762 <sup>8</sup>		103,4		2,730,690 6,554,452 <sup>8</sup>	
	26.	DATE OF	27 DEDIO		LOSS, ACRE-FEE					0,334,432			
			37.1 EKIO	D CAI ACII I	LOSS, ACKE-TEE	<u> </u>		6. TOTAL SEDI	MENT DEPOSITS TO DATE,		E, AF		
	SUK	RVEY a. TO		L	b. AVG. ANN.	c. /MI. <sup>2</sup> -YR.	a	ı. TOTAL	b. AVG. ANN.		c. /MI.	<sup>2</sup> -YR.	
		6/1948		8,028 10	1,070	0.5	506	8,028		1,070		0.509	
		0/1/40			1,070					,		0.507	
	7/1953			5 778 10	1 133	0.5			,			0.521	
				5,778 10	1,133	0.5		13,806		1,096	i	0.521	
		4/1967		5,778 <sup>10</sup> 8,368 <sup>10</sup>	606	0.2	286	22,174		838	5 3	0.398	
	26	4/1967 6/2007	20 AVC 1	5,778 <sup>10</sup> 8,368 <sup>10</sup> 5,575	606 139	0.2 0.0	286 065	22,174 27,749		,	5 3	0.398 0.197	
	26.	4/1967 6/2007 DATE OF	39. AVG. I	5,778 <sup>10</sup> 8,368 <sup>10</sup> 5,575 DRY WT.	606 139	0.2 0.0 TONS/MI. <sup>2</sup> -YR	286 065	22,174	OSS, PCT.	838 417	42 SED	0.398 0.197 IMENT	
		4/1967 6/2007	39. AVG. 1 (#/FT³)	5,778 <sup>10</sup> 8,368 <sup>10</sup> 5,575 DRY WT.	606 139	0.2 0.0 TONS/MI. <sup>2</sup> -YR b. TOTAL	286 065 4	22,174 27,749	OSS, PCT.	838 417 TAL TO	42 SEDI	0.398 0.197 IMENT W, PPM	
		4/1967 6/2007 DATE OF VEY		5,778 <sup>10</sup> 8,368 <sup>10</sup> 5,575 DRY WT.	606 139 40. SED. DEP. a. PERIOD	0.2 0.0 TONS/ML²-YR b. TOTAL TO DATE	286 065 4	22,174 27,749 1. STORAGE L 1. AVG. ANNUAL	OSS, PCT. b. TO DATE	838 417 TAL TO	42 SEDI INFLOV a. PER.	0.398 0.197 IMENT W, PPM . b. TOT.	
		4/1967 6/2007 DATE OF VEY		5,778 <sup>10</sup> 8,368 <sup>10</sup> 5,575 DRY WT.	606 139 40. SED. DEP. a. PERIOD	0.2 0.0 TONS/MI. <sup>2</sup> -YR b. TOTAL TO DATE	286 065 4 a	22,174 27,749 1. STORAGE L 1. AVG. ANNUAL 0.683	OSS, PCT. b. TO DATE	838 417 TAL TO	42 SEDI INFLOV a. PER.	0.398 0.197 IMENT W, PPM b. TOT.	
		4/1967 6/2007 DATE OF VEY 6/1948 7/1953		5,778 <sup>10</sup> 8,368 <sup>10</sup> 5,575 DRY WT.	606 139 40. SED. DEP. a. PERIOD 10 580 10 1,023	0.2 0.0 TONS/ML <sup>2</sup> -YR b. TOTAL TO DATE	286 065 4 a a 580 759	22,174 27,749 -1. STORAGE L a. AVG. ANNUAL 0.683 0.700	OSS, PCT. b. TO DATE	838 417 TAL TO 5.12 8.81	42 SEDI INFLOV a. PER. 7,072 14,673	0.398 0.197 IMENT W, PPM b. TOT. 7,065 9,849	
		4/1967 6/2007 DATE OF VEY 6/1948 7/1953 4/1967		5,778 <sup>10</sup> 8,368 <sup>10</sup> 5,575 DRY WT.	606 139 40. SED. DEP. a. PERIOD	0.2 0.0 TONS/ML <sup>2</sup> -YR b. TOTAL TO DATE	286 065 4 a	22,174 27,749 -1. STORAGE L a. AVG. ANNUAL 0.683 0.700 0.535	OSS, PCT. b. TO DATE	838 417 TAL TO 5.12 8.81 14.12	42 SEDI INFLOV a. PER.	0.398 0.197 IMENT W, PPM b. TOT. 7,065 9,849	
		4/1967 6/2007 DATE OF VEY 6/1948 7/1953		5,778 <sup>10</sup> 8,368 <sup>10</sup> 5,575 DRY WT.	606 139 40. SED. DEP. a. PERIOD 10 580 10 1,023	0.2 0.0 TONS/ML <sup>2</sup> -YR b. TOTAL TO DATE	286 065 4 a a 580 759	22,174 27,749 -1. STORAGE L a. AVG. ANNUAL 0.683 0.700	OSS, PCT. b. TO DATE	838 417 TAL TO 5.12 8.81	42 SEDI INFLOV a. PER. 7,072 14,673	0.398 0.197 IMENT W, PPM b. TOT. 7,065 9,849	
26		4/1967 6/2007 DATE OF VEY 6/1948 7/1953 4/1967 6/2007	(#/FT <sup>3</sup> )	5,778 <sup>10</sup> 8,368 <sup>10</sup> 5,575 DRY WT. ) 52.3 66.9 70.2	606 139 40. SED. DEP. a. PERIOD 10 580 10 1,023 10 472	0.2 0.0 TONS/MI. <sup>2</sup> -YR b. TOTAL TO DATE	286 065 4 a a 580 759 609	22,174 27,749 1. STORAGE L 1. AVG. ANNUAL 0.683 0.700 0.535 0.266	OSS, PCT. b. TO DATE	838 417 TAL TO 5.12 8.81 14.12	42 SEDI INFLOV a. PER. 7,072 14,673	0.398 0.197 IMENT W, PPM b. TOT. 7,065 9,849	
	SUR	4/1967 6/2007 DATE OF VEY 6/1948 7/1953 4/1967 6/2007	(#/FT <sup>3</sup> )	5,778 <sup>10</sup> 8,368 <sup>10</sup> 5,575 DRY WT. ) 52.3 66.9 70.2	606 139 40. SED. DEP. a. PERIOD 10 580 10 1,023	0.2 0.0 TONS/MI. <sup>2</sup> -YR b. TOTAL TO DATE	286 065 4 a a 580 759 609	22,174 27,749 1. STORAGE L 1. AVG. ANNUAL 0.683 0.700 0.535 0.266	OSS, PCT. b. TO DATE	838 417 TAL TO 5.12 8.81 14.12	42 SEDI INFLOV a. PER. 7,072 14,673	0.398 0.197 IMENT W, PPM b. TOT. 7,065 9,849	
DAT	SUR	4/1967 6/2007 DATE OF VEY 6/1948 7/1953 4/1967 6/2007	(#/FT <sup>3</sup> )	5,778 <sup>10</sup> 8,368 <sup>10</sup> 5,575 DRY WT. ) 52.3 66.9 70.2	606 139 40. SED. DEP. a. PERIOD 10 580 10 1,023 10 472	0.2 0.0 0.0 TONS/ML <sup>2</sup> -YR b. TOTAL TO DATE 5	286 065 4 a 580 759 509	22,174 27,749 1. STORAGE L 1. AVG. ANNUAL 0.683 0.700 0.535 0.266	OSS, PCT. b. TO DATE	838 417 TAL TO 5.12 8.81 14.12 17.70	42 SEDI INFLOV a. PER. 7,072 14,673	0.398 0.197 IMENT W, PPM b. TOT. 7,065 9,849	
DAT OF	SUR E	4/1967 6/2007 DATE OF VEY 6/1948 7/1953 4/1967 6/2007	(#/FT <sup>3</sup> )	5,778 <sup>10</sup> 8,368 <sup>10</sup> 5,575 DRY WT. ) 52.3 66.9 70.2	606 139 40. SED. DEP. a. PERIOD 10 580 10 1,023 10 472	0.2 0.0 TONS/MI. <sup>2</sup> -YR b. TOTAL TO DATE	286 065 4 a a 580 759 609	22,174 27,749 1. STORAGE L 1. AVG. ANNUAL 0.683 0.700 0.535 0.266	OSS, PCT. b. TO DATE	838 417 TAL TO 5.12 8.81 14.12	42 SEDI INFLOV a. PER. 7,072 14,673	0.398 0.197 IMENT W, PPM b. TOT. 7,065 9,849	
DAT OF	SUR	4/1967 6/2007 DATE OF VEY 6/1948 7/1953 4/1967 6/2007	(#/FT <sup>3</sup> )	5,778 <sup>10</sup> 8,368 <sup>10</sup> 5,575 DRY WT. ) 52.3 66.9 70.2	606 139 40. SED. DEP. a. PERIOD 10 580 10 1,023 472 E IN FEET BELOW A	O.2 O.0 O.0 TONS/MI. <sup>2</sup> -YR D. TOTAL TO DATE  SOME STATE  AND ABOVE C	286 065 4 a 3580 2559 5609 CREST ELE 30-20	22,174 27,749 21. STORAGE L 20. AVG. ANNUAL 0.683 0.700 0.535 0.266 EVATION	OSS, PCT. b. TO DATE	838 417 TAL TO  5.12 8.81 14.12 17.70  C-5	42 SEDI INFLOV a. PER. 7,072 14,673	0.398 0.197 IMENT W, PPM b. TOT. 7,065 9,849	
DAT OF SUR	SUR	4/1967 6/2007 DATE OF VEY 6/1948 7/1953 4/1967 6/2007	(#/FT <sup>3</sup> )  DESIGNA  62.3-60	5,778 <sup>10</sup> 8,368 <sup>10</sup> 5,575  DRY WT. )  52.3 66.9 70.2  TION RANGI	606 139 40. SED. DEP. a. PERIOD 10 580 10 1,023 10 472 E IN FEET BELOW A	D.2. 0.0 0.0 TONS/ML²-YR b. TOTAL TO DATE  AND ABOVE C  40-30  AL SEDIMENT	286 265 4 a 2580 759 5609 CREST ELE 30-20 F LOCATEI	22,174 27,749 21. STORAGE L  A. AVG. ANNUAL  0.683 0.700 0.535 0.266  EVATION  20-10  D WITHIN DEPTI	OSS, PCT. b. TO DATE	838 417 TAL TO  5.12 8.81 14.12 17.70  C-5	42 SEDI INFLOV a. PER. 7,072 14,673	0.398 0.197 IMENT W, PPM b. TOT. 7,065 9,849	
DAT OF SUR	SUR E E SVEY	4/1967 6/2007 DATE OF VEY 6/1948 7/1953 4/1967 6/2007	(#/FT <sup>3</sup> )  DESIGNA  62.3-60	5,778 <sup>10</sup> 8,368 <sup>10</sup> 5,575  DRY WT. )  52.3 66.9 70.2  TION RANGE	606 139 40. SED. DEP. a. PERIOD 10 580 10 1,023 10 472 E IN FEET BELOW D 50-40 PERCENT OF TOT 8.22	D.2. 0.0 0.0 TONS/ML²-YR b. TOTAL TO DATE  AND ABOVE C  40-30  AL SEDIMENT 28.31	286 265 4 a a 2759 2759 30-20 F LOCATEI 25.96	22,174 27,749 21. STORAGE LI A. AVG. ANNUAL  0.683 0.700 0.535 0.266  EVATION  20-10  D WITHIN DEPTI 22.62	OSS, PCT. b. TO DATE	838 417 TAL TO  5.12 8.81 14.12 17.70  C-5 FION -2.83	42 SEDI INFLOV a. PER. 7,072 14,673	0.398 0.197 IMENT W, PPM b. TOT. 7,065 9,849	
DAT OF SUR 6/1 7/1	SUR E E E E E E E E E E E E E E E E E E E	4/1967 6/2007 DATE OF VEY 6/1948 7/1953 4/1967 6/2007	(#/FT <sup>3</sup> )  DESIGNA  62.3-60  0.01 0.01	5,778 10 8,368 10 5,575 DRY WT. ) 52.3 66.9 70.2 TION RANGI 0 60-50 5.26 3.24	606 139 40. SED. DEP. 1 a. PERIOD 100 580 100 1,023 472 E IN FEET BELOW 0 0 50-40 PERCENT OF TOT 8.22 16.48	O.2 O.0	286 265 4 a a 259 30-20 F LOCATE! 25.96 16.47	22,174 27,749 21. STORAGE LI 2. AVG. ANNUAL  0.683 0.700 0.535 0.266  EVATION  20-10  D WITHIN DEPTI 22.62 14.85	OSS, PCT. b. TO DATE	838 417 TAL TO  5.12 8.81 14.12 17.70  C-5  FION  -2.83 2.99	42 SEDI INFLOV a. PER. 7,072 14,673	0.398 0.197 IMENT W, PPM b. TOT. 7,065 9,849	
DAT OF SUR 6/1 7/1 4/1	SUR E E E E E E E E E E E E E E E E E E E	4/1967 6/2007 DATE OF VEY 6/1948 7/1953 4/1967 6/2007	(#/FT <sup>3</sup> )  DESIGNA  62.3-60  0.01  0.01  0.01	5,778 <sup>10</sup> 8,368 <sup>10</sup> 5,575  DRY WT.  )  52.3 66.9 70.2  CTION RANGE  5.26 3.24 1.99	606 139 40. SED. DEP. a. PERIOD 10 580 10 1,023 472 E IN FEET BELOW A 0 50-40 PERCENT OF TOT 8.22 16.48 13.54	0.2 0.0 0.0 TONS/ML <sup>2</sup> -YR b. TOTAL TO DATE  Solution  40-30  AL SEDIMENT 28.31 26.61 13.71	286 265 4 a a 25,96 16.47 18.92	22,174 27,749 21. STORAGE L  AVG. ANNUAL  0.683 0.700 0.535 0.266  EVATION  20-10  D WITHIN DEPTI 22.62 14.85 20.62	10-C H DESIGNA' 12.44 19.35 20.67	838 417 TAL TO  5.12 8.81 14.12 17.70  C-5  CION  -2.83 2.99 10.54	42 SEDI INFLOV a. PER. 7,072 14,673	0.398 0.197 IMENT W, PPM b. TOT. 7,065 9,849	
OF SUR 6/1 7/1 4/1 6/2	SUR E E E E E E E E E E E E E E E E E E E	4/1967 6/2007 DATE OF VEY 6/1948 7/1953 4/1967 6/2007 43. DEPTH	(#/FT <sup>3</sup> )  DESIGNA  62.3-6(  0.01  0.01  0.01  0.01	5,778 10 8,368 10 5,575 DRY WT. ) 52.3 66.9 70.2 TION RANGI 0 60-50 3.24 1.99	606 139 40. SED. DEP. 1 a. PERIOD 10 580 10 1,023 472 E IN FEET BELOW. 0 50-40 PERCENT OF TOT 8.22 16.48 13.54 16.1	0.2 0.0 0.0 TONS/ML <sup>2</sup> -YR b. TOTAL TO DATE  AND ABOVE C  40-30  AL SEDIMENT 28.31 26.61 13.71 16.0	286 265 4 a 2580 2759 30-20 F LOCATEI 25.96 16.47 18.92 16.2	22,174 27,749 21. STORAGE L  1. AVG. ANNUAL  0.683 0.700 0.535 0.266  EVATION  20-10  D WITHIN DEPTI 22.62 14.85 20.62 17.1	OSS, PCT. b. TO DATE	838 417 TAL TO  5.12 8.81 14.12 17.70  C-5  FION  -2.83 2.99	42 SEDI INFLOV a. PER. 7,072 14,673	0.398 0.197 IMENT W, PPM b. TOT. 7,065 9,849	
DAT OF SUR 6/1 7/1 4/1 6/2 26.	SUR EE 8VEY 948 953 967 2007	4/1967 6/2007 DATE OF VEY 6/1948 7/1953 4/1967 6/2007 43. DEPTH	(#/FT <sup>3</sup> )  DESIGNA  62.3-6(  0.01  0.01  0.01  0.01	5,778 10 8,368 10 5,575 DRY WT. ) 52.3 66.9 70.2 TION RANGI 0 60-50 3.24 1.99	606 139 40. SED. DEP. a. PERIOD 10 580 10 1,023 472 E IN FEET BELOW A 0 50-40 PERCENT OF TOT 8.22 16.48 13.54	0.2 0.0 0.0 TONS/ML <sup>2</sup> -YR b. TOTAL TO DATE  AND ABOVE C  40-30  AL SEDIMENT 28.31 26.61 13.71 16.0	286 265 4 a 2580 2759 30-20 F LOCATEI 25.96 16.47 18.92 16.2	22,174 27,749 21. STORAGE L  1. AVG. ANNUAL  0.683 0.700 0.535 0.266  EVATION  20-10  D WITHIN DEPTI 22.62 14.85 20.62 17.1	10-C H DESIGNA' 12.44 19.35 20.67	838 417 TAL TO  5.12 8.81 14.12 17.70  C-5  CION  -2.83 2.99 10.54	42 SEDI INFLOV a. PER. 7,072 14,673	0.398 0.197 IMENT W, PPM b. TOT. 7,065 9,849	
OF SUR 6/1 7/1 4/1 6/2	SUR EE 8VEY 948 953 967 2007	4/1967 6/2007 DATE OF VEY 6/1948 7/1953 4/1967 6/2007 43. DEPTH	(#/FT <sup>3</sup> )  DESIGNA  62.3-6(  0.01  0.01  0.01  0.01  DESIGNA	5,778 10 8,368 10 5,575 DRY WT. ) 52.3 66.9 70.2 TION RANGI 0 60-50 5.26 3.24 1.99 1.7	606 139 40. SED. DEP. a. PERIOD 10 580 10 1,023 10 472 E IN FEET BELOW A 0 50-40 PERCENT OF TOT 8.22 16.48 13.54 16.1 ENT OF TOTAL ORI	0.2 0.0 0.0 TONS/ML <sup>2</sup> -YR b. TOTAL TO DATE  5 6 AND ABOVE C  40-30 AL SEDIMENT 28.31 26.61 13.71 16.0 GINAL LENGT	286 286 265 4 4 275 275 275 275 275 275 275 275	22,174 27,749 21. STORAGE L  A. AVG. ANNUAL  0.683 0.700 0.535 0.266  EVATION  20-10 D WITHIN DEPTI 22.62 14.85 20.62 17.1 ERVOIR	10-C H DESIGNA' 12.44 19.35 20.67 24.4	838 417 TAL TO  5.12 8.81 14.12 17.70  C-5  COS  COS  10.54 8.5	42 SED INFLOV a. PER. 7,072 14,673 8,213	0.398 0.197 IMENT W, PPM b. TOT. 7.065 9,849 9,113	
DAT OF SUR 6/1 7/1 4/1 6/2 26.	SUR EE 8VEY 948 953 967 2007	4/1967 6/2007 DATE OF VEY 6/1948 7/1953 4/1967 6/2007 43. DEPTH	(#/FT <sup>3</sup> )  DESIGNA  62.3-6(  0.01  0.01  0.01  0.01	5,778 10 8,368 10 5,575 DRY WT. ) 52.3 66.9 70.2 TION RANGI 0 60-50 5.26 3.24 1.99 1.7 ATION PERCE	606 139 40. SED. DEP. a. PERIOD 10 580 10 1,023 10 472 E IN FEET BELOW A 10 50-40 PERCENT OF TOT 8.22 16.48 13.54 16.1 ENT OF TOTAL ORI 80-40 40-50	0.2 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	286 286 265 265 265 275 275 275 275 275 275 275 27	22,174 27,749 21. STORAGE L  A. AVG. ANNUAL  0.683 0.700 0.535 0.266  EVATION  20-10 D WITHIN DEPTI 22.62 14.85 20.62 17.1 ERVOIR  0-80 80-90	10-C h DESIGNA' 12.44 19.35 20.67 24.4	838 417 TAL TO  5.12 8.81 14.12 17.70  C-5  FION  -2.83 2.99 10.54 8.5	42 SEDI INFLOV a. PER. 7,072 14,673	0.398 0.197 IMENT W, PPM b. TOT. 7.065 9,849 9,113	
OF SUR 6/1 7/1 4/1 6/2 26. DAT	SUR  EE  RVEY  948  953  967  0007	4/1967 6/2007 DATE OF VEY 6/1948 7/1953 4/1967 6/2007 43. DEPTH	(#/FT <sup>3</sup> )  DESIGNA  62.3-60  0.01 0.01 0.01 0.01 10-20	5,778 10 8,368 10 5,575 DRY WT. ) 52.3 66.9 70.2 TION RANGI 0 60-50 5.26 3.24 1.99 1.7 ATION PERCE	606 139 40. SED. DEP. a. PERIOD  10 580 10 1,023 10 472  E IN FEET BELOW  D 50-40  PERCENT OF TOT  8.22 16.48 13.54 16.1  ENT OF TOTAL ORI  30-40 40-50  PERCENT OF TOT	0.2 0.0 0.0 TONS/ML <sup>2</sup> -YR b. TOTAL TO DATE  AND ABOVE C  40-30  AL SEDIMENT 16.0 GINAL LENGT  50-60 60 AL SEDIMENT	286 265 4 a a 580 7759 5609  CREST ELE 30-20  F LOCATE 16.2 16.2 TH OF RES 0-70 76 C LOCATE	22,174 27,749 21. STORAGE LI A. AVG. ANNUAL  0.683 0.700 0.535 0.266  EVATION  D WITHIN DEPTI 22.62 14.85 20.62 17.1 ERVOIR  0-80 80-90 D WITHIN REACI	10-C h DESIGNA' 12.44 19.35 20.67 24.4 90-100 h DESIGNA'	838 417 TAL TO  5.12 8.81 14.12 17.70  C-5  FION  -2.83 2.99 10.54 8.5	42 SED INFLOV a. PER. 7,072 14,673 8,213	0.398 0.197 IMENT W, PPM b. TOT. 7.065 9,849 9,113	
DAT OF SUR 6/1 7/1 4/1 6/2 26. DAT	SUR E E E E E E E E E E E E E E E E E E E	4/1967 6/2007 DATE OF VEY 6/1948 7/1953 4/1967 6/2007 43. DEPTH 44. REACH 0-10	(#/FT <sup>3</sup> )  DESIGNA  62.3-66  0.01 0.01 0.01 10-20  4.48	5,778 10 8,368 10 5,575 DRY WT. ) 52.3 66.9 70.2 TION RANGE 0 60-50 3.24 1.99 1.7 ATION PERCE 20-30 3	606 139 40. SED. DEP. a. PERIOD  10 580 10 1,023 10 472  E IN FEET BELOW  PERCENT OF TOT  8.22 16.48 13.54 16.1 ENT OF TOTAL ORI  60-40 40-50 PERCENT OF TOT  11.1 14.42	0.2 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	286 265  4  a  2759 2760  CREST ELE  30-20  F LOCATE  25.96 16.47 18.92 16.2 16.2 16.7 10 F RES  10 TOCATE  10	22,174 27,749 21. STORAGE LA AVG. ANNUAL  0.683 0.700 0.535 0.266  EVATION  D WITHIN DEPTI 22.62 14.85 20.62 17.1 ERVOIR  0-80 0-80 0-90 D WITHIN REACT 1.93 7.93	10-C H DESIGNA 12.44 19.35 20.67 24.4 90-100 H DESIGNA 3.78	838 417 TAL TO  5.12 8.81 14.12 17.70  C-5  FION  -2.83 2.99 10.54 8.5	42 SEDI INFLOV a. PER. 7,072 14,673 8,213	0.398 0.197 IMENT W, PPM b. TOT. 7.065 9,849 9,113	
DAT OF SUR 6/1 7/1 4/1 6/2 26. DAT	SUR  EE  RVEY  948  953  967  0007	4/1967 6/2007 DATE OF VEY 6/1948 7/1953 4/1967 6/2007 43. DEPTH	(#/FT <sup>3</sup> )  DESIGNA  62.3-60  0.01 0.01 0.01 0.01 10-20	5,778 10 8,368 10 5,575 DRY WT. ) 52.3 66.9 70.2 TION RANGE 0 60-50 3.24 1.99 1.7 ATION PERCE 20-30 3	606 139 40. SED. DEP. a. PERIOD  10 580 10 1,023 10 472  E IN FEET BELOW  D 50-40  PERCENT OF TOT  8.22 16.48 13.54 16.1  ENT OF TOTAL ORI  30-40 40-50  PERCENT OF TOT	0.2 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	286 265  4  a  2759 2760  CREST ELE  30-20  F LOCATE  25.96 16.47 18.92 16.2 16.2 16.7 10 F RES  10 TOCATE  10	22,174 27,749 21. STORAGE LI A. AVG. ANNUAL  0.683 0.700 0.535 0.266  EVATION  D WITHIN DEPTI 22.62 14.85 20.62 17.1 ERVOIR  0-80 80-90 D WITHIN REACI	10-C h DESIGNA' 12.44 19.35 20.67 24.4 90-100 h DESIGNA'	838 417 TAL TO  5.12 8.81 14.12 17.70  C-5  FION  -2.83 2.99 10.54 8.5	42 SED INFLOV a. PER. 7,072 14,673 8,213	0.398 0.197 IMENT W, PPM b. TOT. 7.065 9,849 9,113	

Table 1 - Reservoir Sediment Data Summary (page 1 of 2).

45. RANGE IN RESERVOIR OPERATION <sup>8</sup>												
YEAR	MAX. ELEV.	MIN. ELEV.	INFLOW, AF	YEAR	MAX. ELEV.	MIN. ELEV.	INFLOW, AF					
1940-44				1945	1,536.9	1,523.2	59,000					
1946	1,531.2	1,526.9	12,920	1947	1,550.5	1,528.2	160,200					
1948	1,548.0	1,542.0	51,180	1949	1,560.2	1,540.8	139,900					
1950	1,560.4	1,553.5	158,600	1951	1,562.1	1,551.6	213,400					
1952	1,551.8	1,530.8	22,960	1953	1,531.4	1,525.6	15,750					
1954	1,549.6	1,525.6	99,630	1955	1,543.9	1,525.6	57,150					
1956	1,545.0	1,525.8	49,620	1957	1,559.5	1,525.0	122,900					
1958	1,557.9	1,549.4	64,190	1959	1,559.9	1,548.6	120,600					
1960	1,560.0	1,552.5	136,700	1961	1,562.0	1,552.7	188,800					
1962	1,560.1	1,551.8	122,800	1963	1,559.3	1,554.1	62,800					
1964	1,548.2	1,529.3	31,300	1965	1,547.7	1,528.5	79,660					
1966	1,551.7	1,537.7	68,740	1967	1,542.0	1,530.0	42,340					
1968	1,545.0	1,529.9	56,018	1969	1,559.0	1,545.7	116,807					
1970	1,554.0	1,535.9	24,113	1971	1,535.6	1,527.7	11,040					
1972	1,539.4	1,526.8	43,762	1973	1,553.0	1,526.4	102,159					
1974	1,550.3	1,538.0	44,463	1975	1,559.0	1,539.6	129,403					
1976	1,561.8	1,547.9	55,862	1977	1,559.2	1,547.7	243,083					
1978	1,559.1	1,544.1	120,157	1979	1,558.1	1,543.8	90,571					
1980	1,557.5	1,534.4	51,861	1981	1,536.6	1,525.8	13,644					
1982	1,558.0	1,527.0	130,976	1983	1,555.1	1,537.3	49,227					
1984	1,546.0	1,525.3	44,314	1985	1,537.6	1,523.0	37,444					
1986	1,545.5	1,530.0	80,091	1987	1,560.3	1,554.8	345,585					
1988	1,559.5	1,544.6	82,767	1989	1,559.1	1,550.7	232,191					
1990	1,559.9	1,548.3	128,433	1991	1,557.3	1,546.2	66,339					
1992	1,559.5	1,546.0	115,575	1993	1,561.6	1,548.7	168,170					
1994	1,554.2	1,532.4	65,635	1995	1,560.7	1,532.5	214,118					
1996	1,559.2	1,552.0	142,654	1997	1,562.2	1,555.6	383,347					
1998	1,559.5	1,536.0	228,248	1999	1,559.4	1,536.5	136,696					
2000	1,559.7	1,539.0	96,128	2001	1,560.3	1,540.4	148,041					
2002	1,547.2	1,527.2	30,374	2003	1,547.5	1,527.4	76,224					
2004	1,545.3	1,530.7	58,892	2005	1,553.0	1,534.0	105,867					
2006	1,545.5	1,525.5	27,906	2007	1,559.8	1,526.6	175,127					

46. ELEVATIO														
ELEVATION	AREA	CAPACITY	ELEVATION	AREA	CAPACITY	ELEVATION	AREA	CAPACITY						
<u>1940</u>	SURVEY 1		1,496.7	0	0	1,500.0	1	2						
1,505.0	58	116	1,510.0	135	586	1,515.0	678	2,448						
1,517.5	1,073	4,608	1,520.0	1,445	7,732	1,525.0	1,991	16,302						
1,530.0	2,510	27,668	1,535.0	3,013	41,678	1,540.0	3,720	58,718						
1,545.0	4,279	78,704	1,550.0	5,302	102,872	1,555.0	6,007	131,132						
1,559.0	6,772	156,668	1,564.0	7,705	192,842									
2007	SURVEY 11													
1,510.0	0	0	1,512.0	6	6	1,514.0	80	78						
1,515.0	134	185	1,516.0	145	324	1,518.0	307	776						
1,520.0	806	1,889	1,522.0	1,159	3,854	1,524.0	1,438	6,451						
1,525.0	1,603	7,971	1,526.0	1,692	9,619	1,528.0	1,853	13,163						
1,530.0	2,049	17,065	1,532.0	2,276	21,390	1,534.0	2,498	26,165						
1,535.0	2,610	28,719	1,536.0	2,719	31,383	1,538.0	2,954	37,056						
1,540.0	3,180	43,191	1,542.0	3,455	49,826	1,544.0	3,728	57,008						
1,545.0	3,849	60,796	1,546.0	3,970	64,706	1,548.0	4,264	72,940						
1,550.0	4,570	81,774	1,552.0	4,820	91,164	1,554.0	5,053	101,038						
1,556.0	5,362	177,267	1,559.0	6,273	128,919	1,564.0	7,170	162,526						
1,566.67	7,793	182,429	1,570.0	8,678	209,853									

#### 47. REMARKS AND REFERENCES

- 1 1940, 1948, 1953, and 1967 surveys from table 2 of report "The 1967 Altus Reservoir Sediment Survey. (http://www.usbr.gov/pmts/sediment).
- <sup>2</sup> Dam crest elevation 1,564.0, top of parapet wall elevation 1,566.67.
- <sup>3</sup> Uncontrolled spillway crest.
- <sup>4</sup> Maximum water surface includes surcharge, elevation 1,562.0 to 1,564.0, and flood control zone, elevation 1,559.0 and 1,562.0.
  Irrigation capacity includes 4,800 acre-feet of municipal use.
- <sup>5</sup> Date of original survey for new dam over deposits placed behind old dam.
- <sup>6</sup> Values from USGS Water Resources Data book for Oklahoma.
- <sup>7</sup> Bureau of Reclamation's Project Data Book, 1981.
- Mean annual runoff of 104,039 acre-feet from available records, water years 1945 through 2007.
- <sup>9</sup> 2007 underwater survey with limited 2006 and 2008 land surveys generated topography up to elevation 1,556.0. Used 1967 results at elevation 1,567.0 to interpolate areas from elevations 1,556.0 through 1,567.0. The 1967 study interpolated areas from elevations 1,550 through 1,567.0. 2007 surface area at 1,559.0 measured from digitized USGS quad contour modified with new survey data.
- Values from 1940 through 1967 from Table 2 of 1967 Altus Reservoir Sediment Survey report.
- Capacity values computed by Reclamation program, ACAP. Surface area data from elevation 1,510.0 through 1,556.0 from 2007 survey study. Surface area data from 1967 used to project reservoir information above elevation 1,559.0. Note that limited collected above water data was used to adjust the USGS upper reservoir quad contours developed in 1970.
- 48. AGENCY MAKING SURVEY Bureau of Reclamation
  49. AGENCY SUPPLYING DATA Bureau of Reclamation DATE March 2008

Table 1 – Reservoir Sediment Data Summary (page 2 of 2).

#### **Area-Capacity Curves for Altus Reservoir** Area (acres) 8,000 6,400 5,600 4,000 3,200 2,400 1,600 800 0 7,200 4,800 1,570 1,570 1,560 1,560 1,550 1,550 Elevation (feet) 1,540 1,540 1,530 1,530 1,520 1,520 2007 1,510 1,510 **-** 1967 **-** 1953 <del>-</del> 1948 Original 1,500 1,500 20000 40000 60000 80000 100000 120000 140000 160000 180000 200000 0 Capacity (acre-feet)

Figure 28 - Altus Reservoir Area and Capacity Plots

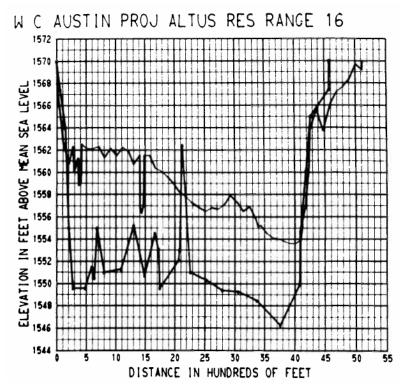


Figure 29 - Range Line 16 (1967 report).

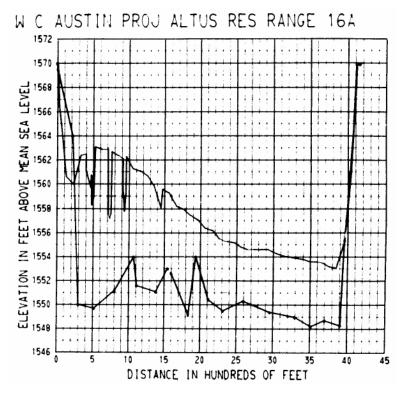


Figure 30 - Range Line 16A (1967 report).

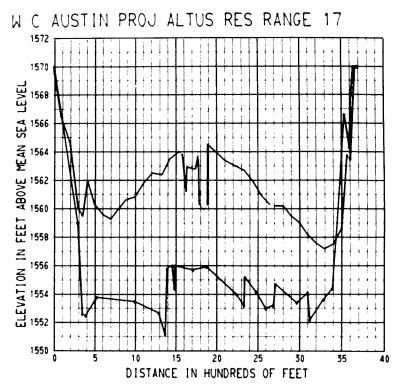


Figure 31 - Range Line 17 (1967 report).

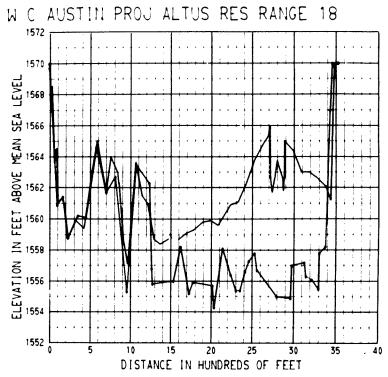


Figure 32 - Range Line 18 (1967 report).

### 2007 Storage Capacity

The storage-elevation relationships based on the measured surface areas were developed using the area-capacity computer program ACAP (Bureau of Reclamation, 1985). The ACAP program can compute the area and capacity at elevation increments from 0.01 to 1.0 foot by linear interpolation between the given contour surface areas. The program begins by testing the initial capacity equation over successive intervals to ensure that the equation fits within an allowable error limit. The error limit was set at 0.000001 for Altus Reservoir. The capacity equation is then used over the full range of intervals fitting within the allowable error limit. For the first interval at which the initial allowable error limit is exceeded, a new capacity equation (integrated from basic area curve over that interval) is utilized until it exceeds the error limit. Thus, the capacity curve is defined by a series of curves, each fitting a certain region of data. Through differentiation of the capacity equations, which are of second order polynomial form, final area equations are derived:

$$y = a_1 + a_2 x + a_3 x^2$$
 where: 
$$y = \text{capacity}$$
 
$$x = \text{elevation above a reference base}$$
 
$$a_1 = \text{intercept}$$
 
$$a_2 \text{ and } a_3 = \text{coefficients}$$

Results of the Altus Reservoir area and capacity computations are listed in a separate set of 2007 area and capacity tables and have been published for the 0.01, 0.1 and 1-foot elevation increments (Bureau of Reclamation, 2007). A description of the computations and coefficients output from the ACAP program is included with these tables. The original, 1948, 1953, 1967, and 2007 area-capacity relationships are listed on table 2 and the curves are plotted on Figure 28. As of June 2007, at conservation use elevation 1,559.0, the surface area was 6,273 acres with a total capacity of 128,919 acre-feet.

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20
						-								. 0	. •				
					1948	1948			1953	1953			1967	1967			2007	2007	
	Original	Original	1948	1948	Sediment	Percent	1953	1953	Sediment	Percent	1967	1967	Sediment	Percent	2007	2007	Sediment	Percent	Percent
Elevation	Area	Capacity	Area	Capacity	Volume	Computed	Area	Capacity	Volume	Computed	Area	Capacity	Volume	Computed	Area	Capacity	Volume	Computed	Reservoir
<u>Feet</u>	Acres	<u>Ac-Ft</u>	Acres	<u>Ac-Ft</u>	<u>Ac-Ft</u>	<u>Sediment</u>	Acres	Ac-Ft	<u>Ac-Ft</u>	<u>Sediment</u>	<u>Acres</u>	<u>Ac-Ft</u>	<u>Ac-Ft</u>	<u>Sediment</u>	Ac-Ft	<u>Ac-Ft</u>	<u>Ac-Ft</u>	<u>Sediment</u>	<u>Depth</u>
1,564	7,705	192,842	7,773	185,035	7,807		7,740	178,610	14,232		7,168	168,063	24,779		7,170	162,526	30,316		100.0
1,559	6,772	156,668	6,793	148,640	8,028	100.0	6,575	142,862	13,806	100.0	6,260	134,494	22,174	100.0	6,273	128,919	27,749	100.0	92.6
1,555	6,007	131,132	5,951	123,178	7,954	99.1	5,769	118,192	12,940	93.7	5,534	110,907	20,225	91.2	5,221	106,175	24,957	89.9	86.6
1,550	5,302	102,872	5,102	95,568	7,304	91.0	4,945	91,433	11,439	82.9	4,626	85,506	17,366	78.3	4,570	81,774	21,098	76.0	79.2
1,547	4,777	87,670	4,543	81,108	6,562	81.7	4,422	77,390	10,280	74.5	4,144	72,350	15,320	69.1	4,117	68,749	18,921	68.2	74.7
1,545	4,279	78,704	4,120	72,444	6,260	78.0	4,124	68,846	9,858	71.4	3,823	64,383	14,321	64.6	3,849	60,796	17,908	64.5	71.8
1,540	3,720	58,718		53,254	5,464	68.1	3,577	49,609	9,109	66.0	3,219	46,778	11,940	53.8	3,180	43,191	15,527	56.0	64.3
1,535	3,103	41,678		37,086	4,592	57.2	2,912	33,415	8,263	59.9	2,616	32,191	9,487	42.8	2,610	28,719	12,959	46.7	56.9
1,530	2,510	27,668	2,270	24,155	3,513	43.8	2,199	20,679	6,989	50.6	2,165	20,240	7,428	33.5	2,049	17,065	10,603	38.2	
1,525	1,991	16,302		14,035	2,267	28.2	1,578	11,280	5,022	36.4	1,645	10,715	-	25.2	1,603	7,971	8,331	30.0	
1,520	1,445	7,732		6,368	1,364	17.0	1,111	4,591	3,141	22.8	1,103	3,845	3,887	17.5	806	1,889	5,843	21.1	34.6
1,517.5	1,073	4,608	922	3,614	994	12.4	735	2,300	2,308	16.7	643	1,663	2,945	13.3	266	633	3,975	14.3	
1,515	678	2,448		1,640	808	10.1	373	940	1,508	10.9	182	632		8.2	134	185	2,263	8.2	
1,510	135	586		100	486	6.1	41	44	542	3.9	59	30		2.5	0	0	586	2.1	
1,505	58	116	0	0	116	1.4	0	0	116	0.8	0	0	116	0.5	0	0	116	0.4	12.3
1,500	1	2	0	0	2	0.0	0	0	2	0.0	0	0	2	0.0	0	0	2	0.0	
1,497	0	0	0	0	0	0.0	0	0	0	0.0	0	0	0	0.0	0	0	0	0.0	0.0
1	Dogozzaia	water surfa	as slovest	don															-
2		eservoir su																	
2		eported res																	
4		voir surfac		ipacity.															
5		voir capaci																	
6				column (3)	) - column (	(5).													
7						ent (8,028 a	cre-feet	at elevati	on 1,559.0).										
8		voir surfac							, , , , , , , ,										
9		voir capaci																	
10				column (3)	) - column (	(9).													
11	1953 measu	red sedimen	t in perc	entage of t	total sedime	ent (13,806 a	acre-feet	at elevat	ion 1,559.0).										
12	1967 reser	voir surfac	e area.																
13	1967 reser	voir capaci	ty recomp	uted using	ACAP.														
14	1967 measu	red sedimen	t volume,	column (3)	) - column (	(13).													
15	1967 measu	red sedimen	t in perc	entage of t	total sedime	ent (22,174 a	acre-feet	at elevat	ion 1,559.0).										
16	2007 measu	red reservo	ir surfac	e area. 20	007 surface	area at ele	vation 1	559.0 deve	loped from US	GS quad contou	ır adjuste	ed with lim	ited land sur	face data.					
17	2007 reser	voir capaci	ty comput	ed using AG	CAP.														
18	2007 measu	red sedimen	t volume,	column (3)	) - column (	[17].													
19	2007 measu	red sedimen	t in perc	entage of t	total sedime	ent (27,749 a	acre-feet	at elevat	ion 1,559.0).										
20	Depth of r	eservoir ex	pressed i	n percentag	ge of total	depth, 67.3	feet, fi	om maximum	water surfac	e 1,564.0.									

Table 2 - Summary of 2007 Survey Results.

## 2007 Reservoir Sediment Analyses

Results of the 2007 Altus Reservoir area and capacity computations are listed in Table 1 and columns 16 and 17 of Table 2. Columns 2 and 3 of Table 2 list the original area and capacity values. The results from the 1948, 1953, and 1967 surveys are also listed on this table. For most of the previous survey data, only limited information was located on how the computations were made, except for the 1967 report that indicated all resurveys were by the range line method. Column 18 lists the capacity differences between the original and 2007 survey results due to sediment deposition. Figure 28 is a plot of the Altus Reservoir surface area and capacity values for all surveys, illustrating the differences. The comparisons show that the total reservoir capacity in 2007 is 30,316 acre-feet less than the original volume at maximum reservoir elevation 1,564.0. It must be noted that the 2007 area and capacity tables were generated assuming no surface area change since the 1967 survey at elevation 1,565.0. The 1967 study made a similar assumption where the surface areas from elevation 1,550.0 to 1,565.0 were projected using the ACAP program that uses a straight line computation method. For the 2007 study, the projection was from elevation 1,559.0 to 1,565.0. Assuming no change at elevation 1,565.0 is probably not entirely accurate, but any loss due to sediment deposition above this elevation is not likely to be significant since the reservoir has never operated above elevation 1,562 and rarely operates above elevation 1,560. The 1967 range line plots did show that the lateral distribution of sediment at the lines located above the Granite Bridge has resulted in a significant build-up of sediment from elevation 1,550.0 and above.

Figure 33 provides a 1998 aerial view of the sediment deposition above the causeway and upstream of the left bank at the Granite Bridge location. The photo shows the water pond behind the causeway and possible small channel flow between the pond and main water body of the reservoir via the bridge. The channel that connects the pond to the main reservoir area was observed during the 2008 land survey. But at the time of the survey, it was dry. On the left side of the photo is the straightened river channel upstream of the bridge which bypasses the upper sediment delta that has developed upstream of the causeway. The original river channel alignment flowed from the east side of the reservoir to the west side and then along the north side of the causeway towards the bridge opening (Figure 3). This new alignment of the river provides a more efficient water delivery route to the main reservoir, especially during low river flows. However, this alignment also allows more inflowing sediments to directly enter the main reservoir area below the bridge. The photo also shows sediment build-up downstream of the causeway where the sediment delta on the left bank is eroded and transported downstream towards the main body by inflows during periods of low reservoir levels. In its current condition, the only means to accurately measure this area is by a detailed above water aerial survey. The 2007 study surveys were hindered by the extensive vegetation that has developed since this 1998 photograph was taken.



Figure 33 - 1998 Aerial View of Altus Reservoir.

During the planning phase for this reservoir, the original estimated 100 year sediment accumulation for Altus Reservoir was 57 percent or around 110,000 acre-feet at maximum pool elevation 1,564.0. This computes to an average annual loss of 1,100 acre-feet. Table 1 lists the results of the 1948 and 1953 surveys that measured an average annual loss between surveys of 1,070 and 1,133 acre-feet respectfully. The 1967 survey measured a reduced average annual loss of 606 acre-feet since the 1953 survey. The 2007 survey measured an even lower average annual loss of 139 acre-feet since the 1967 survey. However, as noted earlier in this report, the 2007 aerial data included the shoreline coves that may have been projected as silted-in during the 1967 analysis. Consequently, data comparisons between the 1967 survey data and the 2007 survey data may be statistically invalid. Over the entire operation period from 1940 through 2007, the computed average annual loss was 417 acre-feet. The different survey and analysis methods between all the studies does not appear to be the main reason for the significant decrease in the calculated annual sediment inflow rate. Further analysis would be required to determine why such a significant drop occurred and why the 2007 study results since dam closure are only about one third of the original projection.

The majority of the future inflowing sediments will enter and settle downstream of the Granite Bridge with the sediment delta growing towards the dam (Figure

4). Future surveys will be needed to measure this growth and to better refine the average annual loss due to sediment.

The results of the 2007 Altus Reservoir study provide up-to-date surface area and capacity information for the entire reservoir. The only feasible means to obtain detailed information for the upper contours, the area above the causeway, and just downstream of the Granite Bridge would be by aerial collection. It is the general consensus that this study had enough information to develop the current surface areas and resulting capacity as presented in this report. Aerial collection would provide more detailed data for full development, but the results should not greatly differ from the 2007 study from elevation 1,559 and below. In general, a large portion of the original available reservoir area upstream of the Granite Bridge has been lost due to sediment deposition. The 1967 study range lines showed this loss occurred during the first 26.4 years of reservoir operation. The 2007 study cross sections illustrate further sediment deposition in this portion of the reservoir, mainly at Range Line 14. Range Lines 14A and 15 measured insignificant change since 1967. Part of this is due to the realignment of the inflowing river where the water and sediment now flow directly into the main reservoir. However, some reservoir operations since 1967 occurred via the original river alignment before it changed in the early 1990's. The 2007 survey did measure some sediment build up at Range Lines 9, 11, and 13, located downstream of the Granite Bridge. However, it was expected that the buildup would have been even greater and extended further downstream if the 1948 and 1967 annual sediment inflow rates had, in fact, continued to occur through 2007.

Since the 1998 aerial photo was taken, significant tree growth has occurred both upstream and just downstream of the causeway during reservoir drawdown due to the drought of the early 2000's. If these areas become clear of vegetation in the future due to tree die off during higher reservoir operations, similar to the Figure 33 photograph, a winter survey should be planned by either aerial or land collection. To obtain good information on current annual sediment inflow, this data would need to be merged with a future underwater survey when the some of the same areas are covered by several feet of water for adequate data overlap. Either way, it is recommended that an additional sediment resurvey be conducted within the next 10-20 years utilizing at minimum the 2007 methodology or better to more accurately determine current sediment inflow rates.

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